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# On the evolution of aspherical perturbations in the universe: an analytical model

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**Abstract.** I study the role of shear fields on the evolution of density perturbations by using an analytical approximate solution for the equations of motion of homogeneous ellipsoids embedded in a homogeneous background. The equations of motion of a homogeneous ellipsoid (Icke 1973; White & Silk 1979 (hereafter WS)) are modified in order to take account of the tidal field as done in Watanabe 1993 and then are integrated analytically, similarly to what done in WS. The comparison of the analytical solution with numerical simulations shows that it is a good approximation to the numerical one. This solution is used to study the evolution of the configuration of the ellipsoids, to calculate the evolution of the density contrast and that of the axial peculiar velocity of the ellipsoids for several values of the amplitude of the external tidal field, and compared again with numerical simulations. In order to calculate the evolution of the density contrast at turn-around and collapse velocity at the epoch of collapse, as a function of the ratio of the initial value of the semi-axes, I use the previously obtained approximate solution to modify the analytical model proposed by Barrow & Silk (1981) for the ellipsoids evolution in the non-linear regime. The density contrast at turn-around and the collapse velocity are found to be reduced with respect to that found by means of the spherical model. The reduction increases with increasing strength of the external tidal field and with increasing initial asymmetry of the ellipsoids. These last calculations are also compared with numerical solutions and they are again in good agreement with the numerical ones.

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**Key words:** cosmology: theory - large scale structure of universe - galaxies: formation

## 1. Introduction

Most clusters and superclusters, similarly to elliptical galaxies, are not spherical and their shape is not due to rotation (Rood et al. 1972; Gregory & Tifft 1976; Dressler 1981). This deviation from spherical symmetry is seen wherever large-scale structures can be unambiguously delineated. Going towards very large scales this tendency to the 'breaking of symmetry' takes the form of strong inhomogeneity and subclustering. For example, the Local Supercluster (LSC) has an appreciable flatness of the axial ratio, 1:6-1:9 (see Tully 1982). On smaller scales, clusters of galaxies are often highly elongated and galaxies are significantly aspherical. In the framework of the gravitational instability, in which structures formed by the gravitational amplification of small primeval inhomogeneities, this lack of spherical symmetry should be somehow expected. In fact, the perturbations that gave rise to the formation of structures are alike to have been initially aspherical (Barrow & Silk 1981 (hereafter BS); Peacock & Heavens 1985; Bardeen et al. 1986) and asphericities are then amplified during gravitational collapse (Lin et al. 1965; Icke 1973; BS). The elongations are probably due to a velocity anisotropy of the galaxies (Aarseth & Binney 1978). According to Binney & Silk (1979) and to Salvador-Solé & Solanes (1993) the elongation of clusters originates in the tidal distortion by neighboring protoclusters. In particular, Salvador-Solé & Solanes (1993) found that the main distortion on a cluster is produced by the nearest neighboring ones having more than 45 galaxies and the same model can explain the observed alignment between neighboring clusters (Binggeli 1982; Oort 1983; Rhee & Katgert 1987; Plionis 1994) and that between clusters and their first ranked galaxy (Carter & Metcalfe 1980; Dressler 1981; Binggeli 1982; Rhee & Katgert 1987; Tucker & Peterson 1988; van Kampen & Rhee 1990; Lambas et al. 1990; West 1994). <sup>1</sup> As previously reported, another characteristic found by some of the studies previously quoted (e.g., Binggeli 1982), is a tendency of clusters through alignment, seen for the first time in two-dimensional distribution of Abell Clusters (Binggeli 1982). The evidences reported suggest that the anisotropy of the external density field plays an important role in the evolution of clusters or superclusters. To be more precise, we should tell that the role of shear on structure formation is of fundamental importance. Shear on a density perturbation can be produced by the intrinsic asphericity of the perturbation itself (internal shear) or it can be due to the interaction of the perturbation with the neighboring ones (external shear) <sup>2</sup> The role of external shear on structure formation was

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<sup>1</sup> Clusters elongations and alignment could be also explained by means of Zeldovich's (1978) "pancakes" theory of cluster formation but this top-down formation model is probably ruled out for several well known reasons (Peebles 1993).

<sup>2</sup> the term "internal shear" has the meaning of "intrinsic asphericity" while "external shear" that of "non-spherical external force".

studied theoretically in Binney & Silk (1979) and Palmer (1983). In particular, Palmer (1983), studied the gravitational collapse of homogeneous prolate spheroids under the influence of a single attractor. The importance of the external shear for structure formation was recognized by Hoffman (1986a, 1989). In particular Hoffman (1986a, 1989), using the quasi-linear (QL) approximation (Zel'dovich 1970; Zel'dovich & Novikov 1983), showed that the shear affects the dynamics of collapsing objects and leads to infall velocities that are larger than in the case of non-shearing ones. As a consequence, according to Hoffmann (1986a, 1989), a general mass element collapse faster than a spherical one. Evrard & Crone (1992), Bertschinger & Jain (1994) and Monaco (1995), arrived at similar conclusions. Bertschinger & Jain (1994) put this result in theorem form according to which spherical perturbations are the slowest in collapsing.

On the actuality of the Bertschinger & Jain's collapse theorem there is not fully agreement in literature. For example, according to the previrialization conjecture (Peebles & Groth 1976, Davis & Peebles 1977, Peebles 1990), initial asphericities and tidal interactions between neighboring density fluctuations induce significant non-radial motions which oppose the collapse. This kind of conclusion was supported by BS, Szalay & Silk (1983), Villumsen & Davis (1986), Bond & Myers (1993a,b) and Lokas et al. (1996). In a more recent paper, Audit et al. (1997) have proposed some analytic prescriptions to compute the collapse time along the second and the third principal axes of an ellipsoid, by means of the 'fuzzy' threshold approach. They pointed out that the formation of virialized clumps must correspond to the third axis collapse and that the collapse along this axis is slowed down by the effect of the shear rather than be accelerated by it, in contrast to its effect on the first axis collapse. They concluded that spherical collapse is the fastest, in disagreement with Bertschinger & Jain's theorem.

Van de Weygaert & Babul (1994) studied the influence of shear fields on the evolution of galactic scale perturbations. They found that the tidal forces induced by large-scale inhomogeneities can affect the mass in and around primordial density peaks and that in some peculiar conditions the shear can break up a primordial peak into two distinct halos. Shear is even able to produce the collapse of a void (van de Weygaert 1996).

Internal shear has been studied by means of collapsing homogeneous ellipsoids (Icke 1973; WS; BS). These models show that the evolution of an *isolated* homogeneous ellipsoid (namely an ellipsoid not exposed to external tidal force) proceeds through a series of uniform ellipsoids, or in other terms the shape of a perturbation does not change much until it acquires a significant overdensity with respect to the background. The collapse time of perturbations of given initial overdensity, decreases with increasing eccentricity and the collapse is faster for near-oblate configurations (than near prolate ones). BS showed that the density contrast at turn-around and the collapse velocity at pancake

formation are reduced relative to the spherical case. Summarizing, the main conclusions are that internal shear can alter the collapse history of structures (Icke 1973; WS). I want to recall that the ellipsoid model has also been used to calculate the cosmological density parameter (WS; BS; Watanabe 1993).

It is important to remark that while the homogeneous ellipsoid model has been widely used in the cosmological context (Palmer 1983; WS; Peebles 1980; BS; Hoffman 1986; Monaco 1995; Eisenstein & Loeb 1995; Bond & Myers 1996a,b; van de Weygaert 1996; Audit & Alimi 1996), only a few papers deal with the study of the effect of shear on the ellipsoid evolution and the analytical studies are even less (WS; BS). Moreover, the effect of internal and external shear has been studied separately: for example WS, BS and Watanabe & Inagaki (1991, 1992) neglect the role of the tidal forces; Watanabe 1993 studied only the effect of external shear.

It is then interesting to study the evolution of the homogeneous ellipsoid taking account of both internal and external shear and to look for analytical solutions of the equations describing the evolution of an ellipsoidal perturbation.

In this paper, I shall study the effect of internal and external shear finding an approximate analytical solution to the equations of motion given in Watanabe (1993). These equations are the equations of Icke (1973) and WS, modified to take account of the effect of the tidal distortion. Similarly to WS, I find an approximate solution to Watanabe's equations which is after compared with numerical simulations.

The paper has fundamentally two aims:

- 1) to find an analytical solution for the equations describing the evolution of an ellipsoidal perturbation and to study the changes in configuration, axial velocity fields, and density contrast in terms of the internal shear (intrinsic initial asphericity) and external shear.
- 2) To study how internal and external shear affect the ellipsoid overdensity at turn-around and axial velocity at the collapse epoch. The final aim is to have some insights in the previrialization conjecture.

I develop this last item by improving BS model, namely I use the analytical solution of the equations of motion, previously found, to calculate the density contrast at turn-around and the axial velocity at the collapse epoch, similarly to what is done by BS.

The plan of the paper is the following: in Sect. 2, I introduce the equations of motion of an *unisolated* ellipsoid. In Sect. 3, I find an approximate analytical solution to the previous equations, similarly to what is done by WS for the *isolated* ellipsoid model. In Sect. 4, I use the previous solution to find the evolution of the density contrast and the axial peculiar velocity. In Sect. 5, the density contrast at turn-around and the velocity at collapse are calculated in order to have some insights on the effects of shear on the collapse of the structure. Sect. 6 is devoted to conclusions.

## 2. Unisolated homogeneous ellipsoid model

The equations of motion of an irrotational homogeneous ellipsoid with semiaxis lengths  $a_1$ ,  $a_2$  and  $a_3$  embedded in a Friedmann-Robertson-Walker background was given by Icke (1973), and WS as:

$$\frac{d^2 a_i}{dt^2} = -2\pi G \left[ \rho_e \alpha_i + \left( \frac{2}{3} - \alpha_i \right) \rho_b \right] a_i \quad (1)$$

where  $R_b$  and  $\rho_b$  are respectively the scale factor and density of the background universe,  $\rho_e$  the density within the ellipsoid. The coefficients  $\alpha_i$  are given by:

$$\alpha_i = a_1 a_2 a_3 \int_0^\infty \frac{d\lambda}{(a_i^2 + \lambda) [(a_1^2 + \lambda)(a_2^2 + \lambda)(a_3^2 + \lambda)]^{\frac{1}{2}}} \quad (2)$$

For the rest of the paper, except section (5), I assume that  $a_1 \leq a_2 \leq a_3$ . Note that  $\alpha_i$  satisfies  $\alpha_1 + \alpha_2 + \alpha_3 = 2$ , condition coming from the Poisson equation. The equations to solve are then Eq. (1) together with Eq. (2) and the cosmological equation for the Friedmann model:

$$\frac{d^2 R_b}{dt^2} = -\frac{4\pi}{3} G \rho_b R_b \quad (3)$$

where  $R_b$  is the scale factor of the background universe, and the equations of the conservation of mass in each region:

$$\rho_e a_1 a_2 a_3 = \text{const} \quad \rho_b a_1 a_2 a_3 = \text{const} \quad (4)$$

Eqs. (1)-(4) describe the evolution of an *isolated* ellipsoid.

Before going further, let us consider the effects of the over-simplifications of the model:

- 1) The ellipsoidal approximation, described by the Eqs. (1)-(4), applies mainly in the immediate vicinity of the density extrema (maxima and minima), where the leading terms in the gravitational potential are the quadratic ones. Previous works (see Eisenstein & Loeb 1995) has shown that the inner region of a perturbation is well approximated by the ellipsoid approximation (Eisenstein & Loeb 1995 apply this model to a variety of mass scales in the range  $10^8 - 10^{15} M_\odot$  and WS to superclusters.)
- 2) The homogeneous *isolated* ellipsoid model does not take account of the role of the tidal forces due to other nearby objects. This problem can be solved as shown in the following of this paper or as shown by Eisenstein & Loeb (1995).
- 3) The homogeneous ellipsoid model does not take account of the inhomogeneity and of the substructure internal to the system. This last item is a natural limitation of the model: by definition, a homogeneous ellipsoid cannot represent the substructure or inhomogeneity of the object. This limitation, from one side, prevents us from treating the distribution of matter and angular momentum within the collapsing object and,

from the other side, has the effect of underestimating the effect of previrialization, and in particular the value of the overdensity at virialization,  $\delta_v$  (Peebles 1990). This means that the effect of the shear on the evolution of the density contrast at turnaround and the velocity at collapse, estimated with the ellipsoid model, is even smaller than what one expects in the collapse of a real protostructure.

4) Another limitation of the model is the effect of the matter in the ellipsoid on the smooth background. One expects that the ellipsoid matter causes the density of its immediate surroundings to deviate from the cosmic mean. Then, as a back reaction, tidal fields due to the perturbed external material should induce departure from homogeneity in the ellipsoid. However, when the density inside the ellipsoid,  $\rho_e$ , is very close to the background density,  $\rho_b$ , this effect is negligibly small (Watanabe & Inagaki 1991; WS), while if  $\rho_e \gg \rho_b$ , the evolution will be determined by its self-gravity (WS). Moreover, numerical simulations have shown that it is a good approximation to ignore departures from homogeneity when one calculates the evolution of the axis ratio (Hui & Bertschinger 1995).

In spite of the uncertainties listed above, the ellipsoid model give a good approximation for the evolution of any object which collapsed in a fairly homogeneous manner (WS; Eisenstein & Loeb 1995).

While it is not possible to take account of inhomogeneity, the homogeneous *isolated* ellipsoid model can be modified in order to take account of external shear as done, for example, by Watanabe (1993). In order to get the quoted goal, one has to get a multipole expansion of the gravitational potential,  $\phi$ . The gravitational potential at time  $t$  and comoving coordinates ( $\mathbf{x}$ ), due to the field outside a comoving radius  $X$  is given by:

$$\phi(\mathbf{x}, t) = \sum_l \phi_l(\mathbf{x}, t) = G\rho_b R_b^2 \sum_l x^l \int_{x' > X} \frac{\delta(\mathbf{x}', t)}{x'^{l+1}} P_l(\mu') d^3 x' \quad (5)$$

where  $P_l$  are the Legendre polynomials. In this paper, as I am primarily concerned with shear, I focus on the quadrupole ( $l = 2$ ) terms. In fact, the monopole component,  $l = 0$ , generates no force, since the potential is spatially constant, while the dipole component,  $l = 1$ , induces only streaming motions that cannot alter the shape or induce any rotation. As shown by Eisenstein & Loeb (1995), in the standard CDM scenario, the dipole is generated at large scales, so the object I am studying and its neighborhood move as bulk flow with the consequence that the angular distribution of matter is very small, and then the dipole terms can be ignored. The quadrupole term,  $l = 2$ , is the first term dealing with the effect of tidal distortion:

$$\phi_2(\mathbf{x}, t) = \frac{3}{2} G\rho_b R_b^2 Q_{ij} x_i x_j \quad (6)$$

where the quadrupole tensor,  $Q_{ij}$ , is given by:

$$Q_{ij} = \int \frac{\delta(\mathbf{x}', t)}{x'^5} \left[ x'_i x'_j - \frac{1}{3} \delta_{ij} \mathbf{x}'^2 \right] d^3 x' \quad (7)$$

The quadrupole tensor,  $Q_{ij}$ , is a traceless  $3 \times 3$  matrix, that can be diagonalized using an appropriate coordinate transformation to get:

$$Q_{ij} = Q \begin{pmatrix} -\beta & 0 & 0 \\ 0 & \beta - 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad 1/2 \leq \beta \leq 1 \quad (8)$$

In the following, I assume that the field does not vary significantly during the ellipsoid evolution and consequently, for simplicity, the value of  $\beta$  is assumed to be constant in time (Watanabe 1993; van de Weygaert 1996). For a positive value of  $Q$ , which is the component with maximum absolute value in the quadrupole tensor, a perturbation evolves to a prolate configuration and to an oblate one for a negative value of  $Q$ . If the initial perturbation is spherically symmetric, it shall evolve to an ellipsoid, if all the three components of the quadrupole tensor are different, while, if two components of the quadrupole tensor are equal and  $Q > 0$  the resulting figure is a prolate spheroid or an oblate one if  $Q < 0$ . If the initial perturbation is an ellipsoid, also in the case that the quadrupole tensor has two equal components, the final configuration is an ellipsoid. In fact, though the cluster becomes a spheroid if the two axes of the external perturbations are equal in Watanabe's (1993) model (because he assumed the initial configuration to be spherical symmetric) generally, the external perturbations are triaxial so the cluster remains a figure of ellipsoid if the initial directions of axes of the cluster coincides with those of external perturbations.

The equations of motion are obtained by adding the force due to the potential given by Eq. (6) into Eq. (1). Assuming that the principal axes of the external tidal tensor are always oriented along the principal axes of the mass tensor, the evolution equations reduces to three equations for the three semiaxes of the ellipsoid and are given by (Watanabe 1993; van de Weygaert 1996):

$$\begin{aligned} \frac{d^2 a_i}{dt^2} = & -2\pi G \left\{ \rho_e (\alpha_i - \gamma b_i) + \left[ \frac{2}{3} - (\alpha_i - \gamma b_i) \right] \rho_b \right\} a_i = \\ & -2\pi G \left[ \rho_e \alpha_i + \left( \frac{2}{3} - \alpha_i \right) \rho_b \right] a_i - 2\pi G \gamma (-b_i) (\rho_e - \rho_b) a_i \end{aligned} \quad (9)$$

where:

$$\gamma = \frac{3}{2\pi} \frac{Q}{\delta}, \quad \mathbf{b} = (-\beta, \beta - 1, 1) \quad (10)$$

Note that in the rightmost term of Eq. (9), I wrote  $-b_i$  to display the equation in the same form of van de Weygaert (1996), in order to simplify the comparison with the result of that paper. A comparison of Eq. (1) with Eq. (9) shows that the evolution of the

ellipsoid is modified by the tidal force if the term  $\gamma b_i$  is large, while the evolution of the ellipsoid is dominated by self-gravity if this term is small. I implicitly assume that the external structures, giving rise to the tidal field, are at large distance from the ellipsoid (see Eisenstein & Loeb 1995). As a consequence, the amplitude of the external quadrupole force is assumed to increase with the linear growth rate (Ryden 1988; Watanabe 1993; Eisenstein & Loeb 1995),  $D(t)$  (this last quantity is given in Peebles 1980):

$$Q(t) = Q_0 \frac{D(t)}{D_0} \quad (11)$$

Here the subscript “0” means that the corresponding quantity is calculated at the present epoch and  $D(t) = R_b(t)$ , for an Einstein-de Sitter (hereafter EdS) universe. Similarly to WS, I assume that initially  $R_b = 1$ . In the particular case of an *isolated* ellipsoid with  $a_1 : a_2 : a_3 = 1 : 1.25 : 1.5$ ,  $R_b = 873$  at collapse. For sake of precision, I want to stress that in an Einstein-de Sitter universe, Eq. (11),  $Q(t) = Q_0 \frac{R_b(t_0)(t/t_0)^{2/3}}{R_b(t_0)}$  reduces to  $Q(t_0) = Q_0$  at present time,  $t_0$ .

In order to have an estimate of the value of  $Q_0$ , for a cluster interacting with a neighboring one, I use the simple model in Watanabe (1993). I consider a cluster which has a neighboring cluster with a mean density contrast  $<\delta> \simeq 3$ , a comoving separation  $(0, 0, x_3)$ , and a comoving size  $\Delta x_3 = x_3/3$ . The  $Q_{33}$  quadrupole component is given by:

$$Q_{33} \simeq \frac{8}{9}\pi <\delta> \left(\frac{\Delta x_3}{x_3}\right)^3 \simeq 0.3 \quad (12)$$

The previous estimate corresponds to a cluster interacting with a neighbor having mass excess comparable to that of the Virgo cluster, and separation three times its size.

Another way of estimating  $Q_0$  is by using the anisotropy of the velocity field in the LSC from data of Lilje, Yahil & Jones (1986). If we indicate with  $Q_{v0}$  the component of the largest absolute value of the anisotropic velocity, one gets:  $Q_0 \Omega_0^{0.6} = \frac{4\pi}{3} Q_{v0}$  (Watanabe 1993). Since Lilje, Yahil & Jones (1986) deduced a value of  $Q_{v0} \sim 0.1 - 0.2$  at the distance of the Local Group from Virgo, we have that  $Q_0 \Omega_0^{0.6} \sim 0.4 - 0.8$ .

Before going on, it is important to discuss a basic difference between the present paper and that of Watanabe (1993). Differently from Watanabe (1993), in this paper I assume that protostructures have an initial asphericity, while the paper of Watanabe (1993) (similarly to those of van de Weigaert (1996) and Palmer (1983)) assume that the initial configuration is spherical, so that the principal axes of the external tidal tensor will be oriented along the principal axes of the mass tensor and the equations of motions reduces to three equations involving the diagonal components of the traceless tidal tensor. Our assumption of initial asphericity of protostructures, is motivated by the fact that previous analyzes of the topology of the constant-density profiles in the neighborhood of the peaks of the Gaussian field showed that the isodensity surfaces are simply connected and approximately ellipsoidal (Doroshkevich 1970; Bardeen 1986). We also know that the



initial asphericity has a certain role in shaping the final configuration of the structure (Icke 1973; WS; BS). By means of the assumption, we have the noteworthy advantage of studying the joint effect of “internal and external shear” (see the final part of Sect. (3) for a discussion). The approach of this paper, assuming that the principal axes of the external tidal tensor are always oriented along the principal axes of the mass tensor, is dictated by reasons of mathematical simplicity. I must tell that, at the same time, the assumption is not strange or without motivation: for example van de Weygaert & Babul 1994, in order to study the effect of shear fields on the evolution of galactic scale density peaks, do a similar assumption, namely that the shear tensor, at the location of the peak representing the structure, is oriented so that it is diagonal. Moreover in a recent paper Porciani, Dekel & Hoffman (2002) find a strong alignment between the principal axes of the inertia and shear tensor, in contradiction to usual assumption that the two tensors are largely uncorrelated (Hoffman 1986b; Heavens & Peacock 1988; Catelan & Theuns 1996).

Finally, I want to stress that the approximate solution found in the present paper give a more general representation of structure formation than those described, as examples, in the following sections. For example, the assumptions and results of Watanabe (1993) are re-obtained assuming that the three axes of the ellipsoid are equal, or in other words Watanabe’s result is a “particular case” of those of this paper when  $a_1(t_i) = a_2(t_i) = a_3(t_i)$ . Moreover, in the present paper, I get analytical solutions for the equations of motion of the ellipsoid, while Watanabe (1993) solve the same equations numerically.

### 3. An analytical approximate solution

An analytical approximation of the solution describing the evolution of the  $i$  –  $th$  axis of the *isolated* ellipsoid was found by WS. The equations of motion can be integrated analytically if one assumes that:

- 1) The evolution of the configuration is self-similar, which means that  $\alpha_i(t) \simeq \alpha_i(t_i)$ .
- 2) The time dependence of  $\rho_e a_i$  and  $\rho_b a_i$  are the same as the spherical model, namely:

$$(\rho_e a_i)(t) = \frac{-3}{4\pi G} \ddot{R}_s \frac{R_b(t_i)}{R_s(t_i)} = \frac{-3}{4\pi G} \ddot{R}_e \frac{R_b(t_i)}{R_e(t_i)} \quad (13)$$

where  $R_s$  is the radius of a spherical shell whose initial density enhancement within  $a_s$  is  $\delta_s(t_i) = \delta_e(t_i)$  and

$$(\rho_b a_i)(t) = \frac{-3}{4\pi G} \ddot{R}_b \frac{a_i(t_i)}{R_b(t_i)} \quad (14)$$

Defining  $R_s(t_i) = R_b(t_i) = 1$ , and substituting Eqs.(13)-(14) into Eq. (1) and integrating, one obtains:

$$\frac{a_i(t)}{a_i(t_i)} = R_b - \frac{3}{2} \alpha_i (R_b - R_e) \quad (15)$$

(WS). This approximation gives a good representation for the evolution of the semiaxes of the ellipsoid for configurations not too extreme. A comparison between the numerical solution of the equations of motion, obtained using a Bulirsch-Stoer scheme, and the prediction of Eq. (15) is shown in Fig. 1a-1c. In all the cases studied, the ellipsoids are embedded in an EdS background universe with Hubble parameter  $H_0 = 50 \text{ km/s/Mpc}$  and  $\rho_e/\rho_b = 1.003$ . The velocity perturbation is taken to correspond to the growing mode solution of the linear perturbation theory. Calculations are terminated when the shortest axis becomes zero. In

Fig. 1a-1c, the ellipsoids have initial axial ratios of  $a_1 : a_2 : a_3 = 1 : 1.25 : 1.5$ ,  $1 : 1.5 : 3$ ,  $1 : 1.5 : 5$ , respectively. The solid lines represent the result of the numerical solutions and the dotted lines the approximate analytical solution (Eq. (15)). The top line represent the longest axis evolution and the bottom one that of the shortest one. In this section, I am principally interested in testing the goodness of the approximation and less in describing the general properties of the evolution of the perturbation, a point which was widely discussed in WS and several other papers. However, two interesting points, that emerge from the calculation are worth noting:

- a) the shape of a perturbation is conserved until it acquires a significant overdensity with respect to the background.
- b) The collapse time of perturbations of fixed initial overdensity, for a fixed background, decreases with increasing initial asymmetry. In other words the internal shear influences the collapsing region geometry. More anisotropic initial configurations are characterized by an acceleration of the collapse along the shortest axis and a slowing down along the longest one. As we shall see later, a similar effect is produced by the external shear.

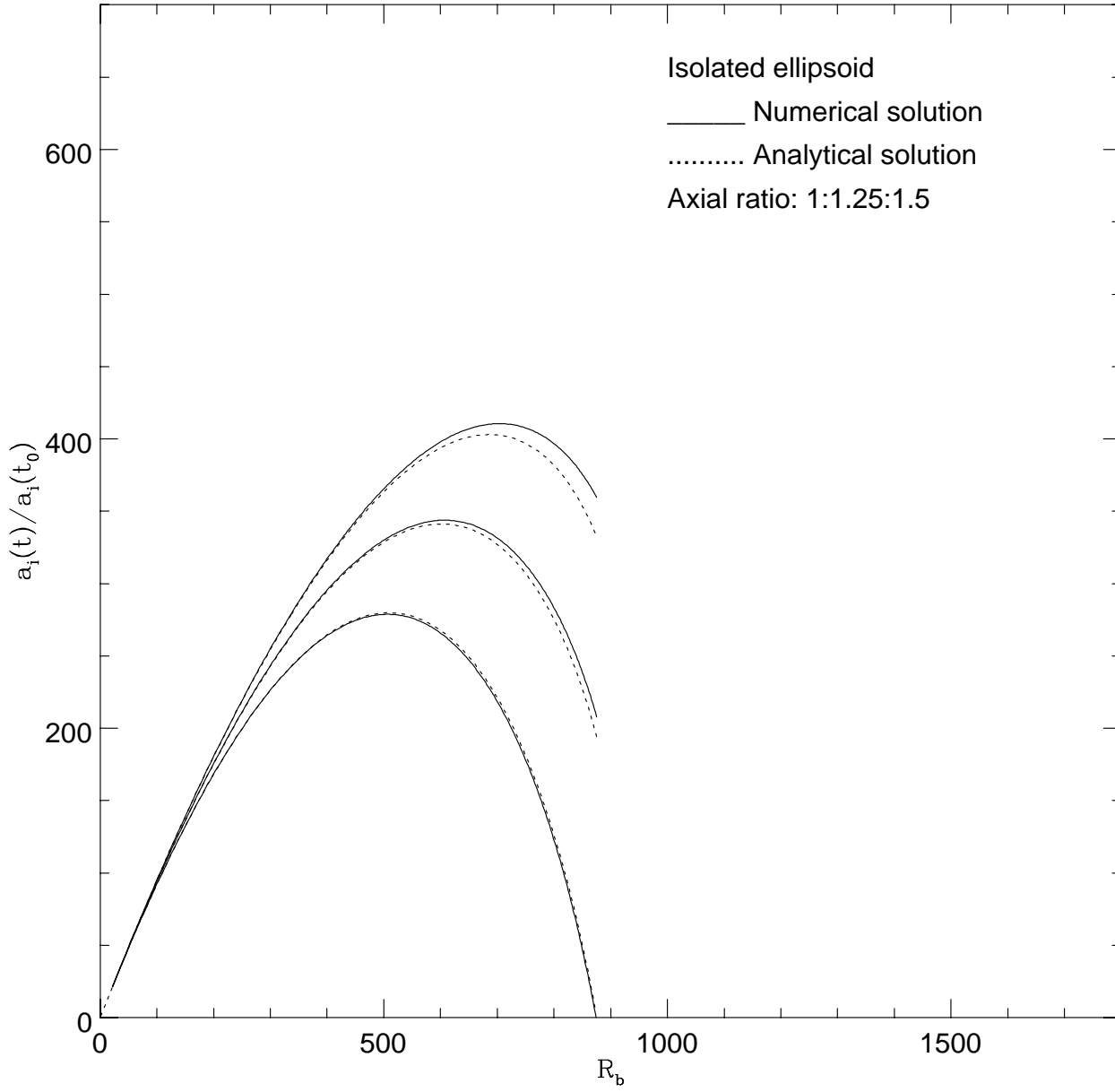
Coming back to the goodness of the approximation of Eq. (15) we have, for example, in the first case ( $a_1 : a_2 : a_3 = 1 : 1.25 : 1.5$ ), that the error in  $a_2(t_c)$  is  $\simeq 7\%$  while that in  $a_3(t_c)$  is  $\simeq 8\%$ , where  $t_c$  is the collapse time of the first axis. For a configuration  $a_1 : a_2 : a_3 = 1 : 1.5 : 3$ , Fig. 1b shows that Eq. (15) gives a worse approximation going from less asymmetric to more asymmetric configurations, especially in the case of the shortest axis. This trend is confirmed by Fig. 1c, representing the initial configuration  $a_1 : a_2 : a_3 = 1 : 1.5 : 5$ . The same problem was encountered by Watanabe & Inagaki (1991) in the calculation of the axial peculiar velocity using WS approximate solution.

It is possible to improve the approximation modifying Eq.(15) slightly, and introducing some parameters whose values can be obtained using the least-square method:

$$\frac{a_1(t)}{a_1(t_i)} = R_b - \frac{3}{2}\alpha_1 (R_b - R_e) - d \times R_b^{\left(\frac{2+3c_1}{2}\right)} \left(1 - \frac{3\alpha_1}{2}\right) \quad (16)$$

$$\frac{a_2(t)}{a_2(t_i)} = R_b - \frac{3}{2}c_2\alpha_2 (R_b - R_e) \quad (17)$$

$$\frac{a_3(t)}{a_3(t_i)} = R_b - \frac{3}{2}c_3\alpha_3 (R_b - R_e) \quad (18)$$

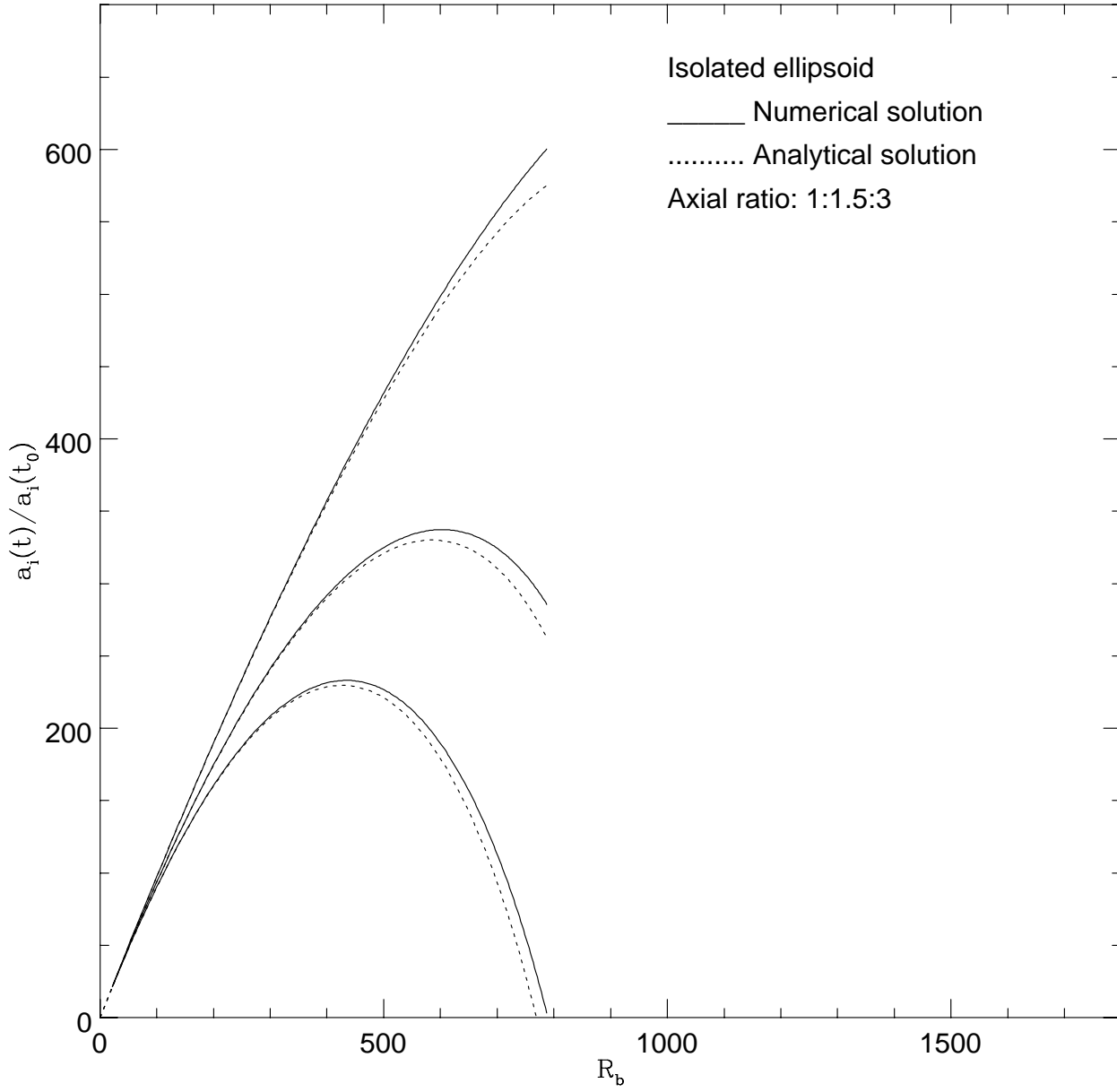


**Fig. 1a** Evolution of *isolated* homogeneous ellipsoidal perturbations in an EdS universe with  $H_0 = 50 \text{ km/s/Mpc}$ ,  $\rho_e/\rho_b = 1.003$  and axial ratio  $1 : 1.25 : 1.5$ . The solid lines represent numerical solutions obtained using Bulirsh-Stoer algorithm while the dotted ones the approximate analytical solution of WS.

For ellipsoids having an initial axial ratio  $1 : a_2 : a_3$  with  $a_1 \geq 1.25$  and  $a_2 \geq 1.5$ , we have that  $d = 7.22 \times 10^{-7}$  and  $c_i$  is given by:

$$c_1 = a_{10}^{-0.115} a_{20}^{0.035} a_{30}^{0.08}, \quad c_2 = a_{10}^{0.07} a_{20}^{-0.06} a_{30}^{-0.01}, \quad c_3 = 1.002 a_{10}^{0.1} a_{20}^{-0.035} a_{30}^{-0.065} \quad (19)$$

where  $a_{i0}$  represents the initial value of the  $i$ -th axis.

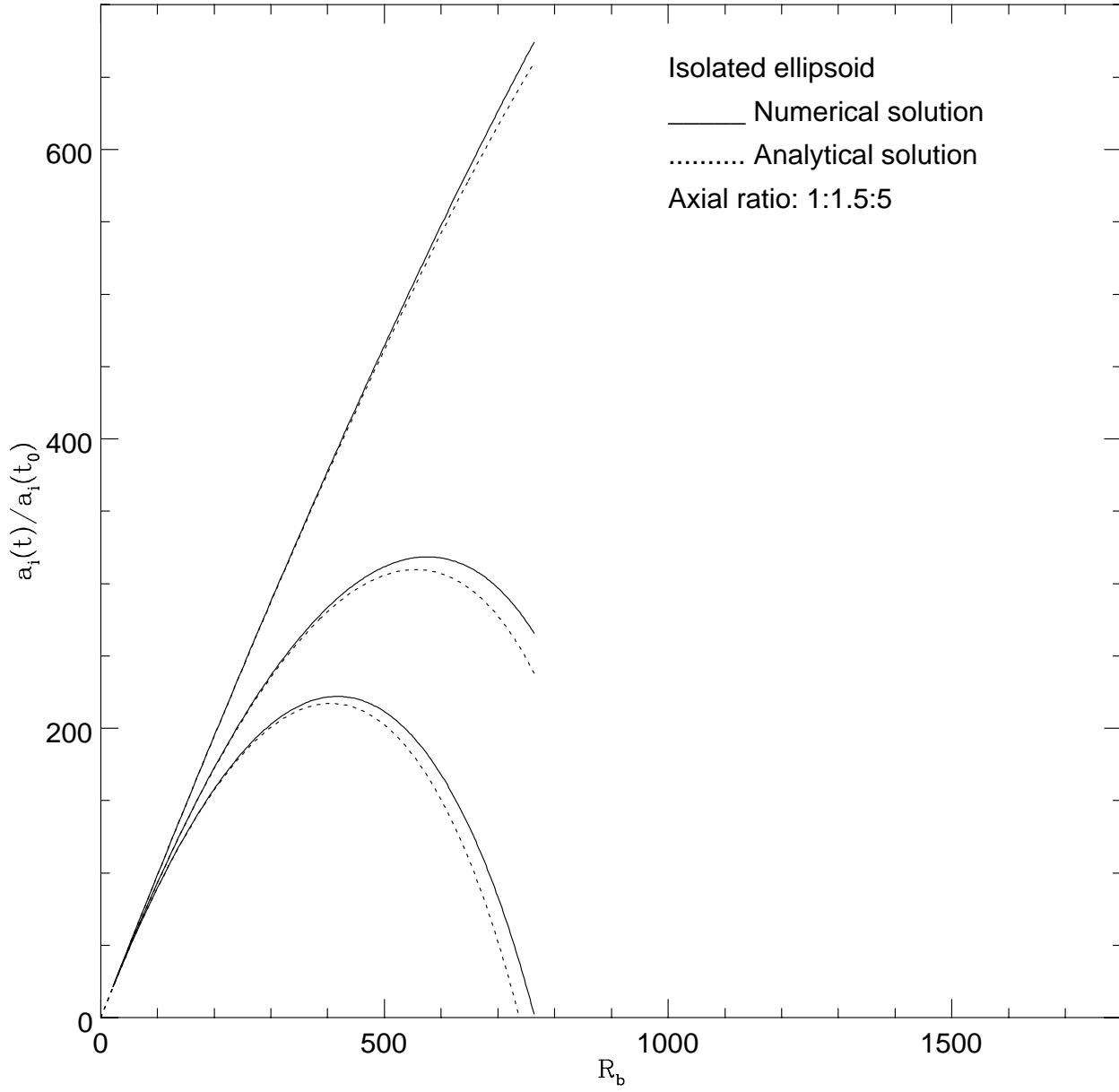


**Fig. 1b** Same as Fig. 1a but now the axial ratio is 1 : 1.5 : 3.

Fig. 1d-1f shows that Eqs. (16)-(18) give a better representation of numerical results, with respect to Eq. (15), for all of the three axes (the initial axial ratio is the same as Figs. 1a-1c).

Similarly to the case of an *isolated* ellipsoid, it is possible to obtain an analytical solution of Eq. (9), describing the evolution of an *unisolated* ellipsoid. In this case the solution can be written in the form:

$$\frac{a_1(t)}{a_1(t_i)} = R_b - \frac{3}{2} \tilde{\alpha}_1 (R_b - R_e) - d \times R_b^{\left(\frac{2+3c_1}{2}\right)} \left(1 - \frac{3\tilde{\alpha}_1}{2}\right) \quad (20)$$



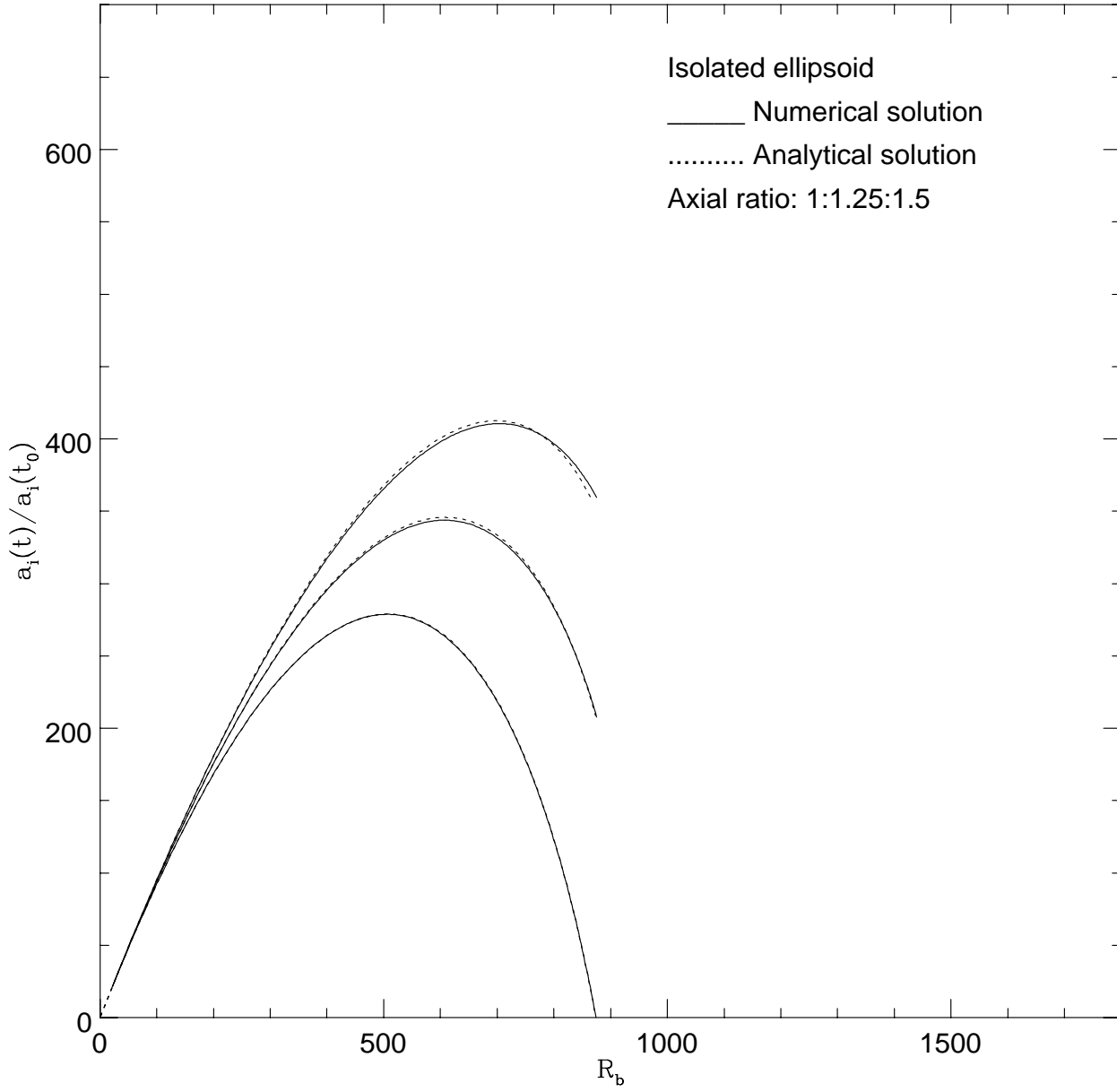
**Fig. 1c** Same as Fig. 1a but now the axial ratio is 1 : 1.5 : 5.

$$\frac{a_2(t)}{a_2(t_i)} = R_b - \frac{3}{2} \tilde{\alpha}_2 (R_b - R_e) \quad (21)$$

$$\frac{a_3(t)}{a_3(t_i)} = R_b - \frac{3}{2} \tilde{\alpha}_3 (R_b - R_e) \quad (22)$$

For ellipsoids having initial axial ratio 1 :  $a_2$  :  $a_3$ , with  $a_1 \geq 1.25$  and  $a_2 \geq 1.5$ , we now have that  $c_1 = 1.23$ ,  $d = 6 \times 10^{-7}$  and:

$$\tilde{\alpha}_1 = \alpha_1 + 0.0672 \left( \frac{b_1}{b_2} \right)^{0.15} b_3^{0.6} \quad (23)$$

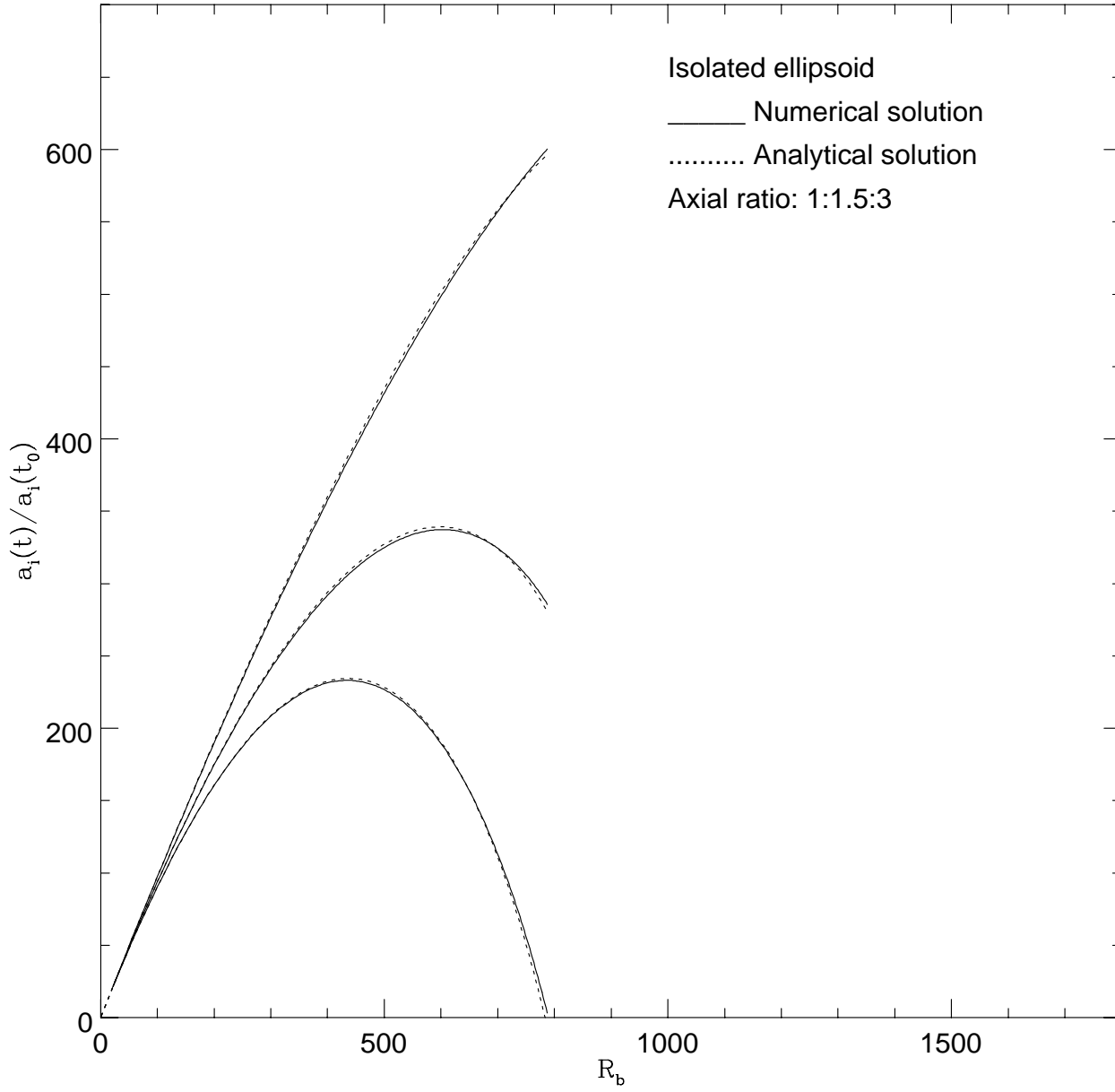


**Fig. 1d** Same as the previous figure Fig. 1a but now the WS analytical approximate solution is improved by using some free parameters fitted to the numerical solution by means of the least-square method (see text for a description).

$$\tilde{\alpha}_2 = a_{10}^{0.07} a_{20}^{-0.06} a_{30}^{-0.01} \left[ \alpha_2 + 0.031 \left( \frac{b_2}{b_1} \right)^{0.5} b_3^{0.95} \right] \quad (24)$$

$$\tilde{\alpha}_3 = 1.002 a_{10}^{0.1} a_{20}^{-0.035} a_{30}^{-0.065} (\alpha_3 - 0.063 a_{30}^{0.09} b_3^{0.95}) \quad (25)$$

where  $b_i$  was defined in Eq. (10).

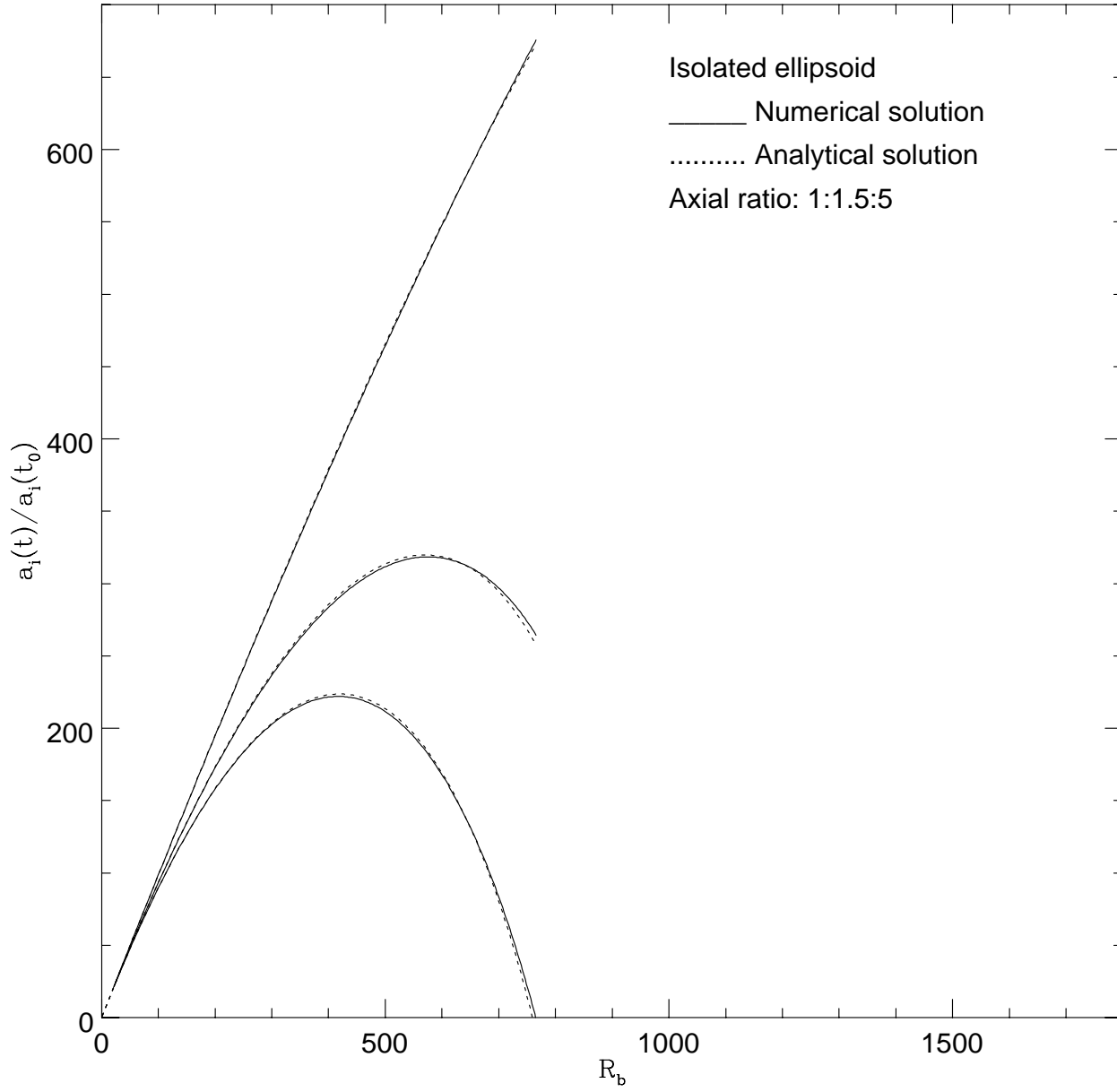


**Fig. 1e** Same as the previous figure Fig. 1b but now the WS analytical approximate solution is improved by using some free parameters fitted to the numerical solution by means of the least-square method (see text for a description).

In the case of prolate spheroids, with axial ratio  $1 : 1 : a_3$  and  $1 \leq a_3 \leq 5$ , a better approximation to the  $\alpha_i$  is:

$$\tilde{\alpha}_1 = \alpha_1 + 0.037 \left( \frac{a_{30}}{a_{10}} \right)^{0.35} \left( \frac{b_1}{b_2} \right)^{0.15} b_3^{0.6} \quad (26)$$

$$\tilde{\alpha}_2 = \left( \frac{a_{10}}{a_{30}} \right)^{0.01} \left[ \alpha_2 + 0.031 \left( \frac{a_{10}}{a_{30}} \right) \left( \frac{b_2}{b_1} \right)^{0.5} b_3^{0.95} \right] \quad (27)$$

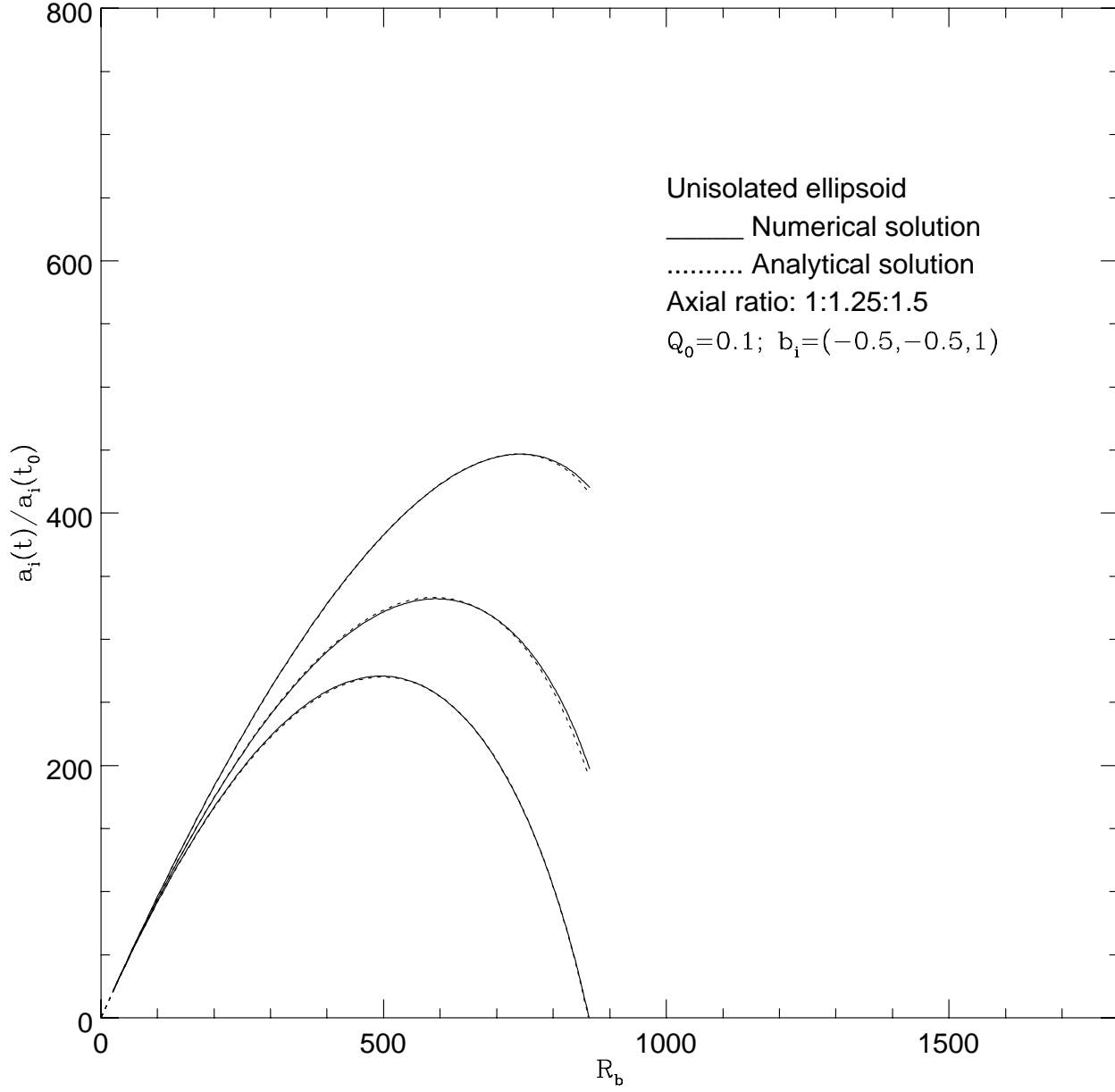


**Fig. 1f** Same as the previous figure Fig. 1c but now the WS analytical approximate solution is improved by using some free parameters fitted to the numerical solution by means of the least-square method (see text for a description).

$$\tilde{\alpha}_3 = 1.002 \left( \frac{a_{20}}{a_{30}} \right)^{0.065} (\alpha_3 - 0.063 a_{30}^{0.09} b_3^{0.95}) \quad (28)$$

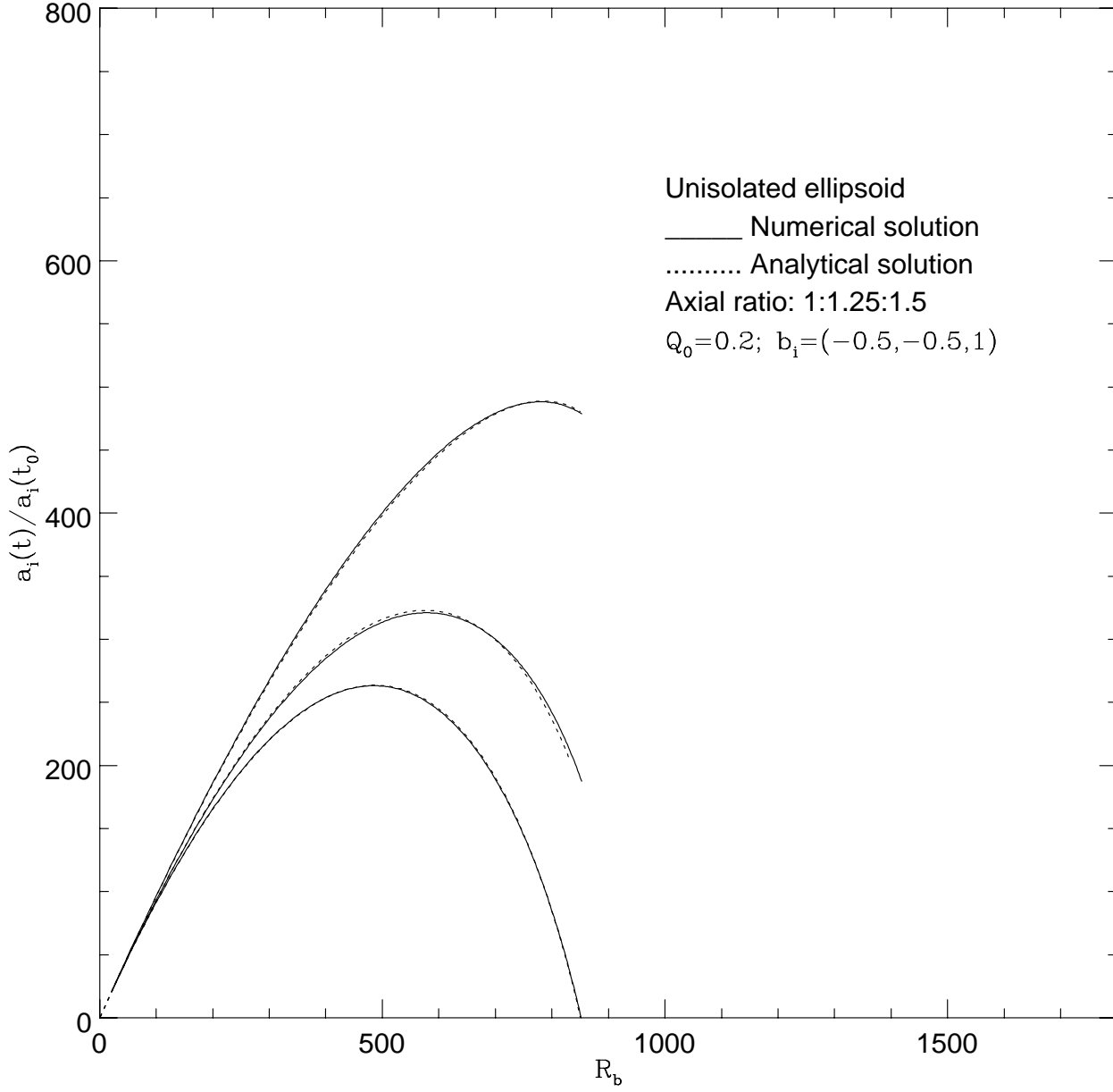
The comparison between the numerical results and Eqs. (20)-(22) are shown in Figs. 2a-2c (the notation in Figs. 2a-2c is the same as fig. 1a-1f). In Figs. 2a-2c, I study the evolution of an ellipsoid having initial axes in the ratio 1 : 1.25 : 1.5 for different values of  $Q_0$ , and  $b_i$  ( $b_i = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.1, 0.2, 0.4$ ). These figures show that for a fixed





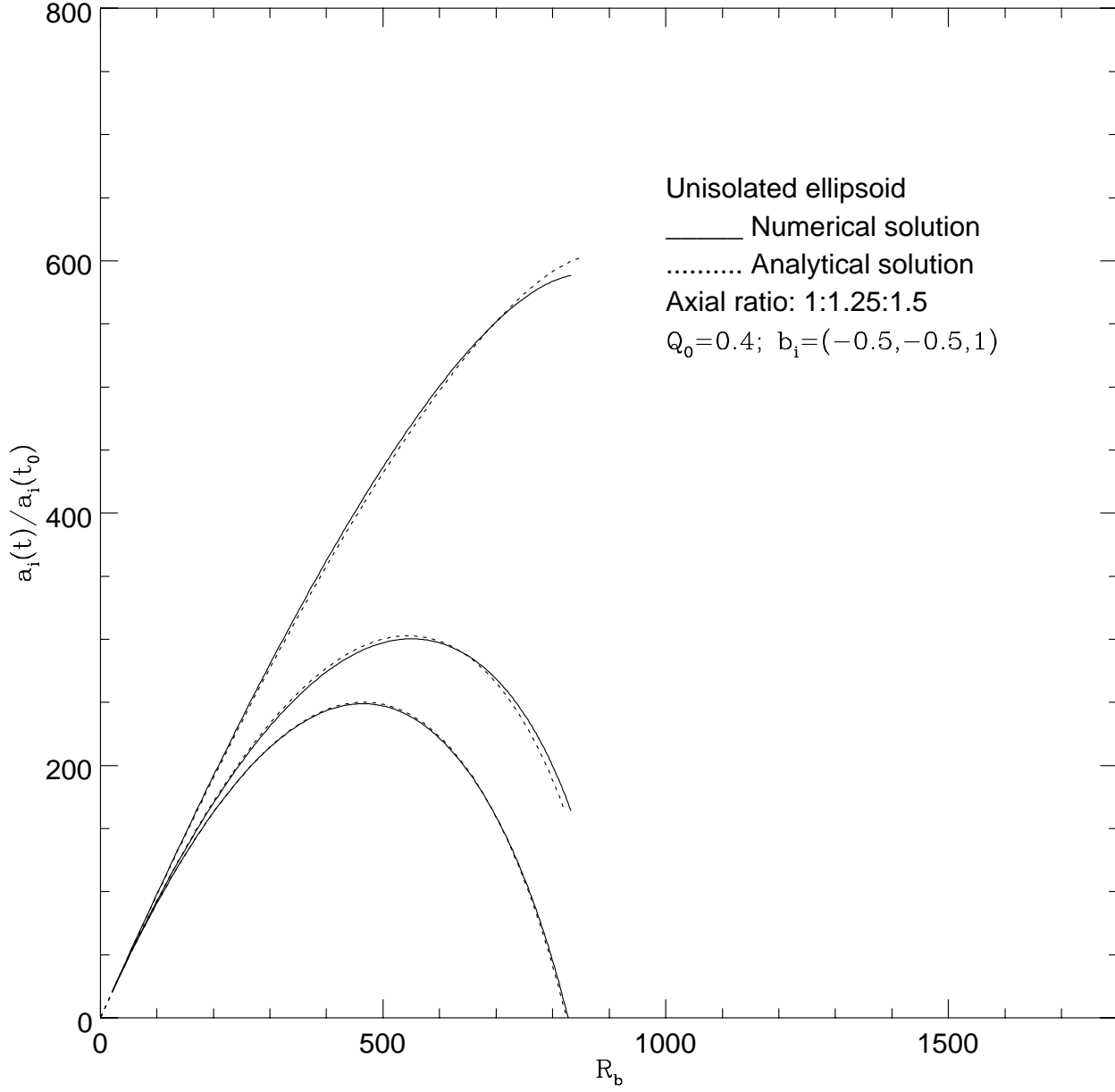
**Fig. 2a** Evolution of *unisolated* homogeneous ellipsoidal perturbations in an EdS universe with  $H_0 = 50 \text{ km/s/Mpc}$ ,  $\rho_e/\rho_b = 1.003$ , axial ratio is  $1 : 1.25 : 1.5$ ,  $b_i = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.1$ .

initial configuration the effect of the external tidal field causes a qualitatively different evolution with respect to an *isolated* ellipsoid. The ellipsoid expands less rapidly along the  $x$  and  $y$  axes, due to the extra decelerating effect of the positive tidal components ( $-b_i = (0.5, 0.5, -1)$ ), and more rapidly along the  $z$  axis, since the tidal force is negative along this axis, and this effect increases with increasing strength of the external tidal field. Summarizing, the effect of a positive tidal force along a given axis is to slow down



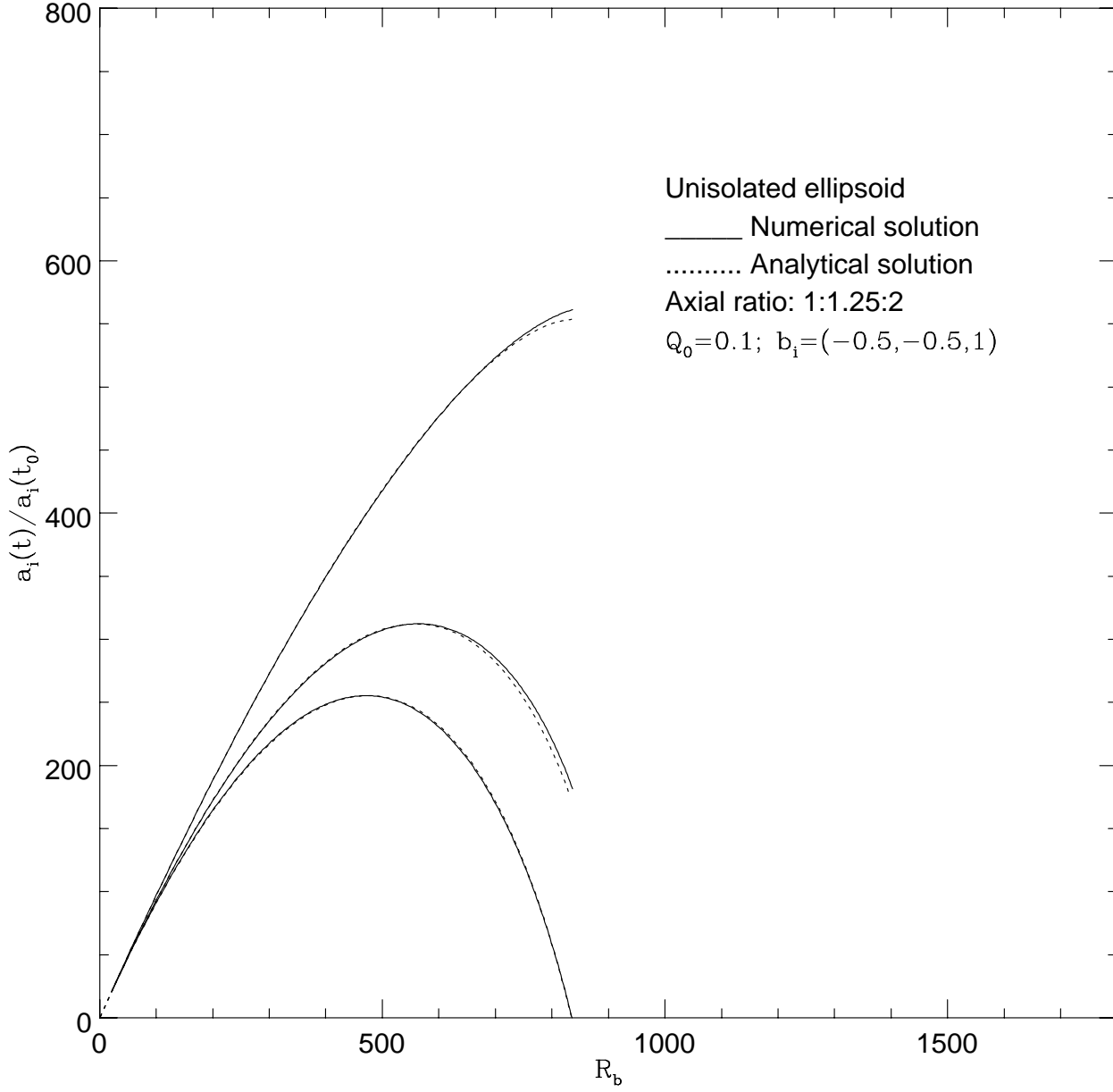
**Fig. 2b** Same as Fig. 2a but now  $Q_0 = 0.2$

the expansion of the ellipsoid along this axis, and the effect of a negative tidal field is to accelerate the expansion of the ellipsoid along that axis. In other words, shear produce dilation in one direction and contraction in the other two and vice versa (contraction in one direction and dilation in the other two), according to its configuration. The result is in agreement with van de Weygaert (1996) and Audit et al. (1997) (note that Eq. (9) and Eq. (1) of van de Weygaert (1996) differ for the sign of the tidal tensor components, such that the evolution of the axes results inverted with respect to our model). One



**Fig. 2c** Same as Fig. 2a but now  $Q_0 = 0.4$

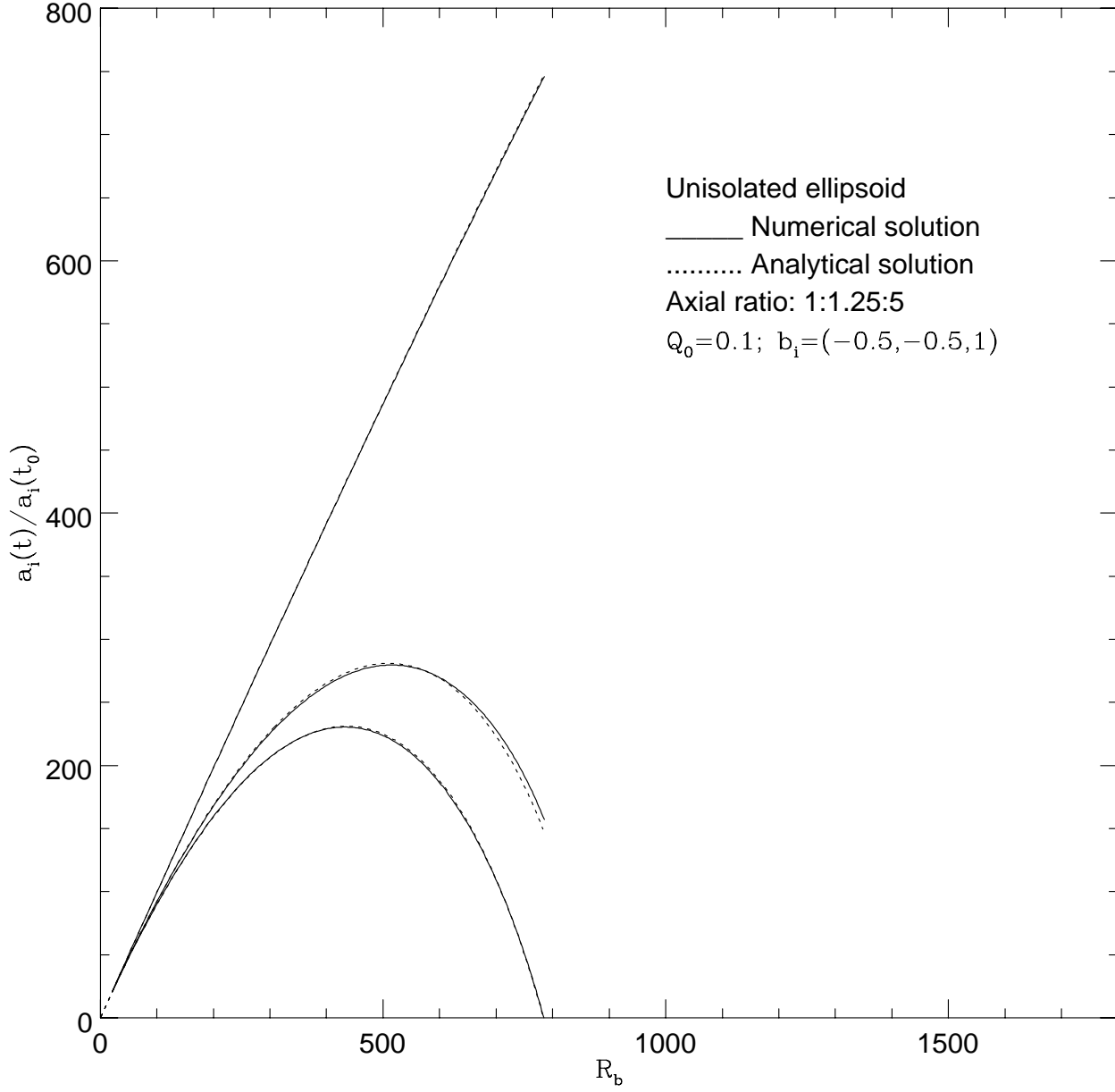
may expect that the shear can change the nature of the secondary infall, influencing the final mass acquired by a peak and the density profiles of halos (Bond & Myers 1993; van de Weygaert & Babul 1994). This idea is confirmed by Figs. 2a-2c, which show that the shear produces a decrease in the collapse time of perturbations of fixed initial overdensity, for a fixed background, and that the effect increases with increasing strength of the external field. It is natural to expect that, for some shear configurations and strong enough external field, even the core region of a perturbation can be induced to fragment,



**Fig. 2d** Same as the previous figure 2a but now the axial ratio is 1 : 1.25 : 2, while  $Q_0 = 0.1$  and  $b_i = (-0.5, -0.5, 1)$ .

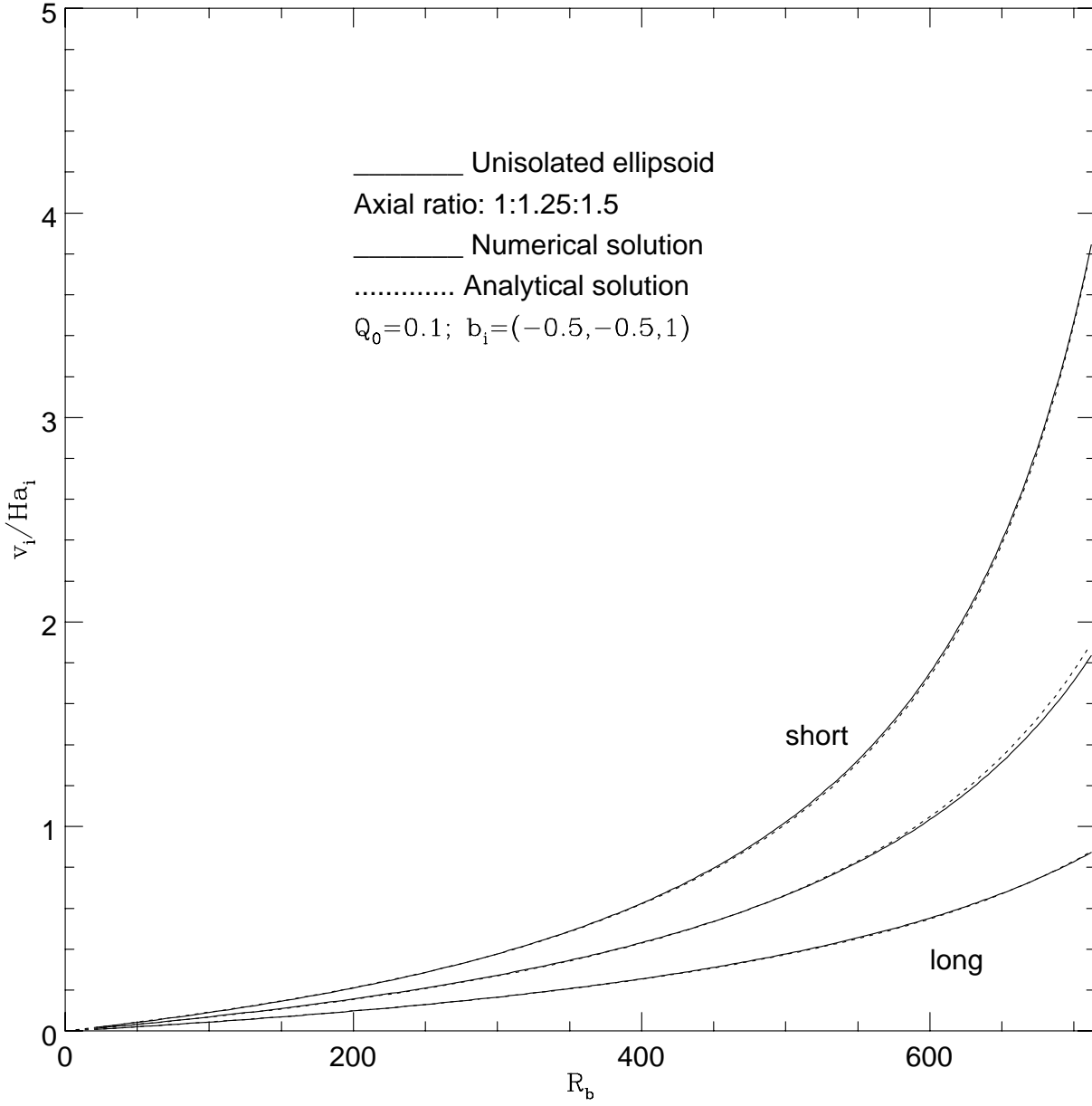
giving rise to different halos (van de Weygaert & Babul 1994), or, as shown by van de Weygaert (1996) and Audit et al. (1997), the external tidal field can induce even a void to collapse, if the external field is strong enough.

In Figs. 2d-2e, I plot the evolution of the ellipsoids for a fixed value of  $Q_0$  and  $b_i$  and for different values of the initial axial ratio, in order to study the effect of the internal shear. In Figs. 2d-2e, the axial ratio is 1 : 1.25 : 2, 1 : 1.25 : 5, respectively,



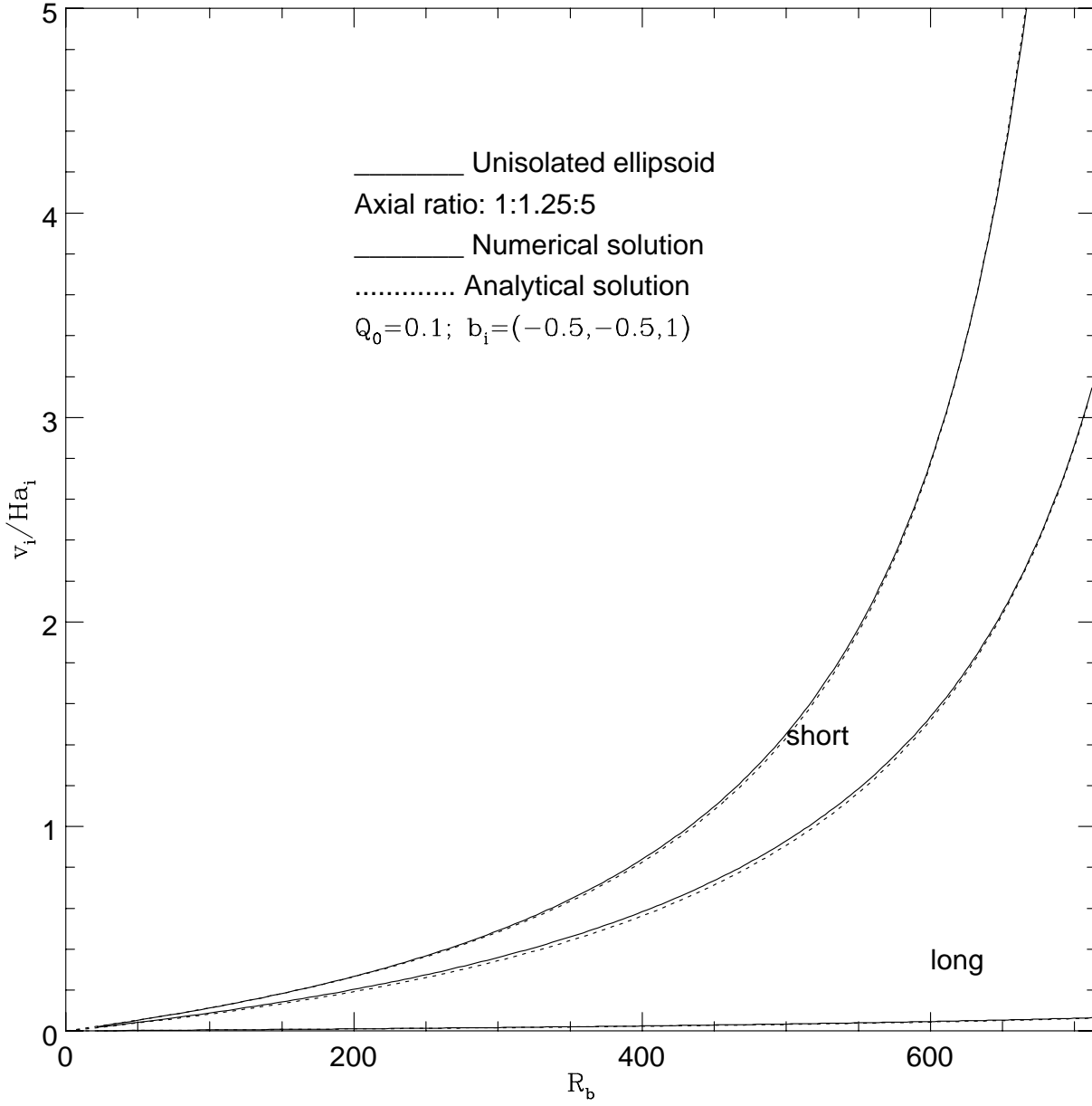
**Fig. 2e** Same as the previous figure 2a but now the axial ratio is 1 : 1.25 : 5, while  $Q_0 = 0.1$  and  $b_i = (-0.5, -0.5, 1)$ .

$Q_0 = 0.1$  and  $b_i = (-0.5, -0.5, 1)$ . The plots show a situation similar to that seen in the case of external shear: namely, the collapse time of the perturbation decreases with increasing initial anisotropy. While for *isolated* ellipsoids or for *unisolated* ones with small values of  $|\gamma|$ , the axial ratio does not appreciably change until the perturbation enters a strongly nonlinear regime, (the self-gravity is dominant), for large values of  $|\gamma|$ , the collapse is anisotropic even for not large values of  $\delta$ . This means that the collapsing



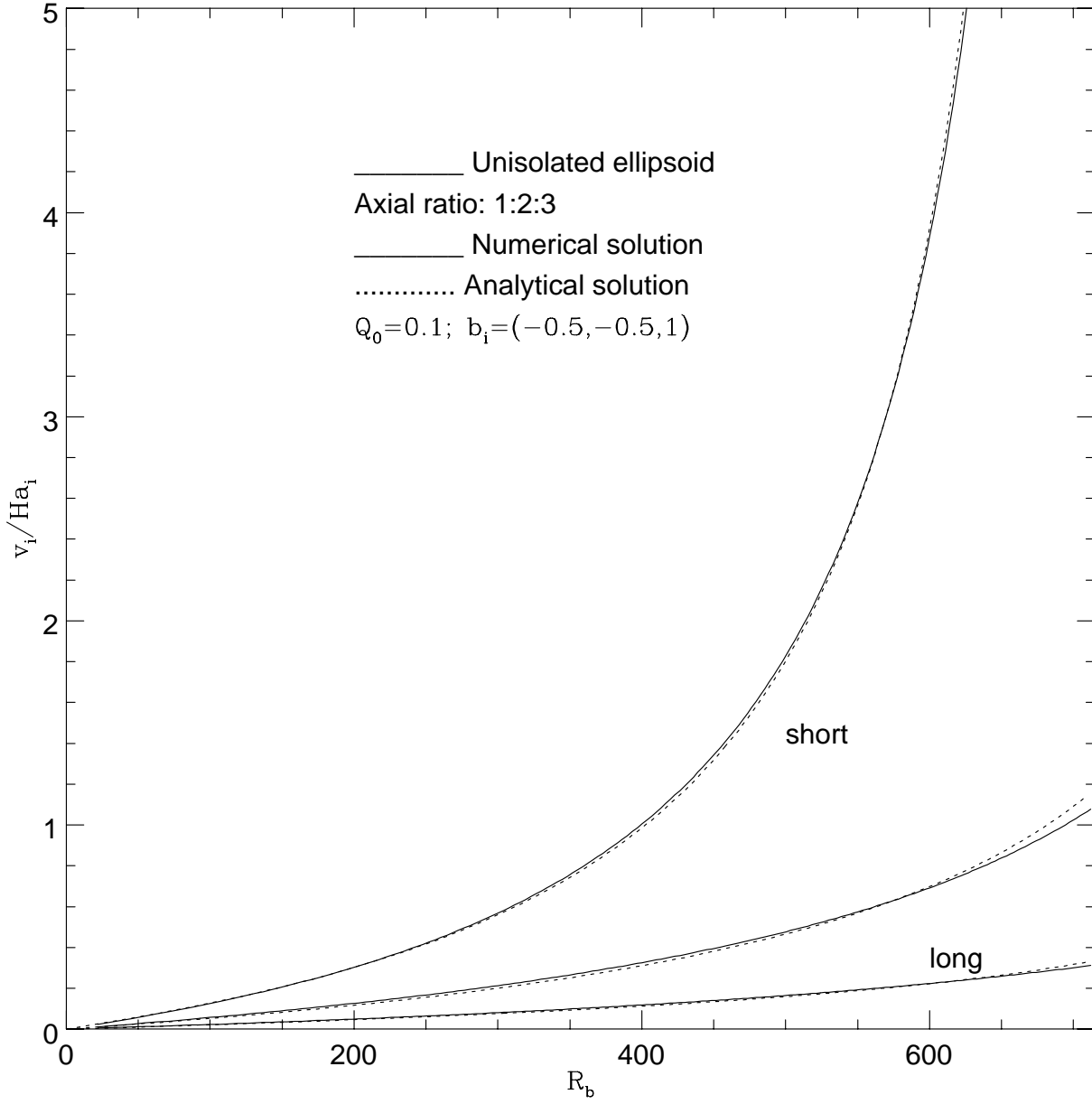
**Fig. 3a** Evolution of the axial velocity. The solid lines represent, from up to bottom, the numerical result for the peculiar velocity along the shortest, medium and longest axis. The dotted line represents the velocity obtained from Eq. (31) using the approximation for the semiaxes (Eqs. (22)-(24)). The value of the axial ratio is 1 : 1.25 : 1.5, while  $Q_0 = 0.1$ , and  $b_i = (-0.5, -0.5, 1)$ .

region geometry is strongly influenced by the external shear. If the external field is strong enough, the external shear is dominant in shaping the region, with respect to internal shear, in agreement with Eisenstein & Loeb (1995), Watanabe(1993).



**Fig. 3b** Same as Fig. 3a but now the value of the axial ratio is 1 : 1.25 : 5, while  $Q_0 = 0.1$ , and  $b_i = (-0.5, -0.5, 1)$ .

As discussed in Sect. (2), in this paper, differently from Watanabe (1993), I assume that protostructures have an initial asphericity. By means of this assumption, I have the noteworthy advantage of being able to study the joint effect of “internal and external shear”. So it is interesting to analyse the contribution to the asphericity of real clusters of galaxies (e.g. LSC), coming from inner shear and external shear. In the case of an



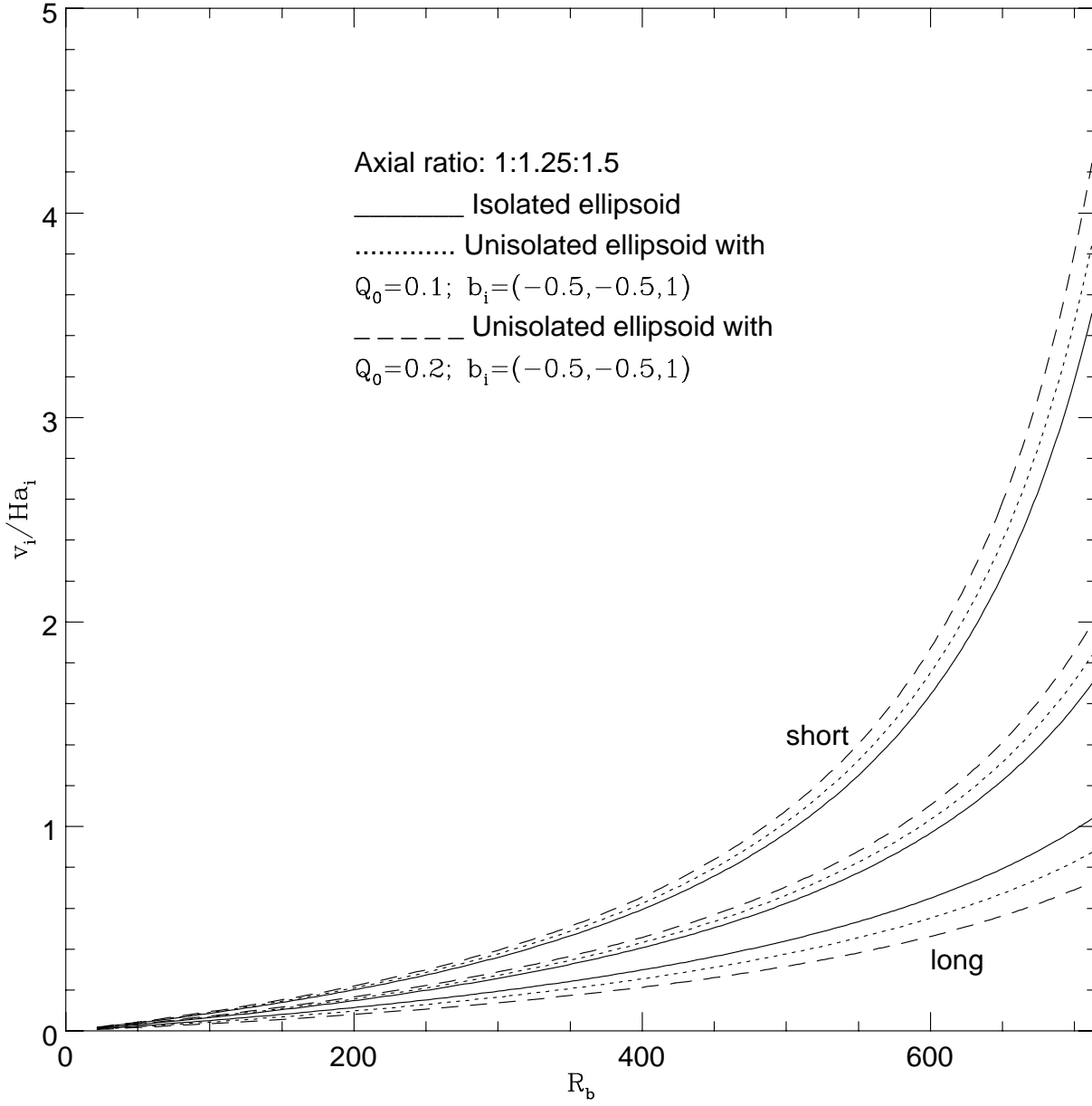
**Fig. 3c** Same as Fig. 3a but now the value of the axial ratio is 1 : 2 : 3, while  $Q_0 = 0.1$ , and  $b_i = (-0.5, -0.5, 1)$ .

*isolated* ellipsoid the length of the uncollapsed axes at collapse can be obtained similarly to WS, by means of Eq. (17)-(18):

$$\frac{a_3(t_c)}{a_2(t_c)} = \frac{a_3(t_i)}{a_2(t_i)} \frac{R_b - \frac{3}{2}c_3\alpha_3(R_b - R_e)}{R_b - \frac{3}{2}c_2\alpha_2(R_b - R_e)} \quad (29)$$

where  $t_c$  is obtained by  $a_1(t_c) = 0$ . Notice that the approximation given in WS (Eq. 11 or Eq. 13) is not very accurate for extreme configurations.

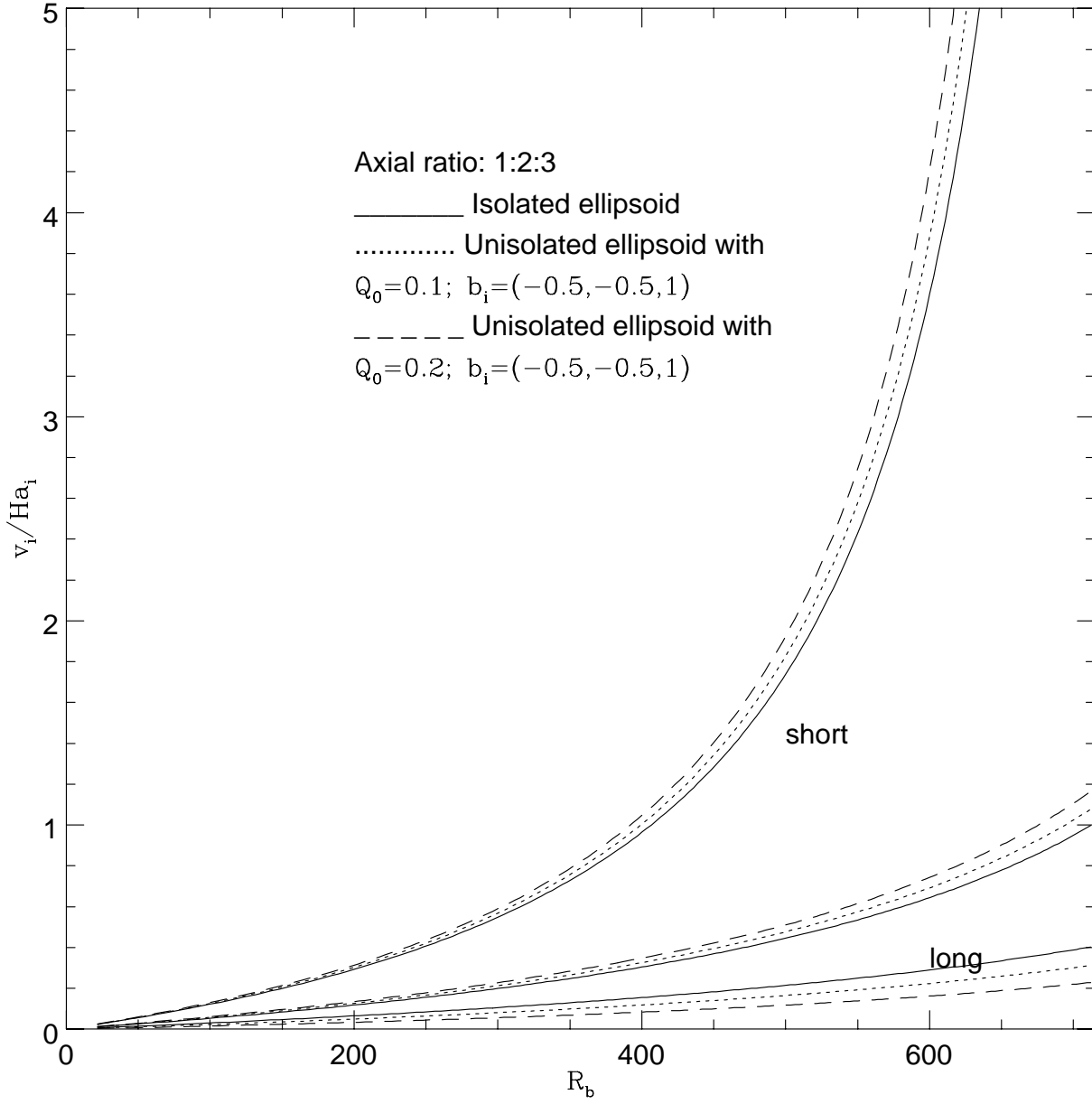




**Fig. 3d** Evolution of the axial velocity. The solid line represents the peculiar velocity for an ellipsoid of axial ratio 1 : 1.25 : 1.5 when no external field is present, while the dotted and dashed lines represent the case  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.2$ ,  $b_i = (-0.5, -0.5, 1)$ , respectively.

In the case of an *unisolated* ellipsoid the length of the uncollapsed axes at collapse can be obtained by means of Eq. (21)-(22):

$$\frac{a_3(t_c)}{a_2(t_c)} = \frac{a_3(t_i)}{a_2(t_i)} \frac{R_b - \frac{3}{2}\tilde{\alpha}_3(R_b - R_e)}{R_b - \frac{3}{2}\tilde{\alpha}_2(R_b - R_e)} \quad (30)$$



**Fig. 3e** Same as Fig. 3d, but now the axial ratio is 1 : 2 : 3.

If we consider an initial *isolated* ellipsoid with  $a_1 : a_2 : a_3 = 1 : 1.25 : 1.5$ , I get at collapse a ratio  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 1.9$ . For the same initial axial ratio and  $b = (-0.5, -0.5, 1)$ ,  $Q_0 = 0.1$ , I get  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 2.5$  which produces an increase of  $\simeq 34\%$  on the previous ratio. Increasing the value of  $Q_0$  to 0.2 implies that  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 3.3$  and so an increase of  $\simeq 76\%$  on the previous ratio. If  $Q_0 = 0.4$ , I get  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 5.9$ , indicating a dominant role of external shear in shaping structures for high  $Q_0$ . We can study the effect of varying the initial configuration of ellipsoids in presence of external shear. In the case of an

**Table 1.** Lengths of the uncollapsed axes at collapse for different values of external and internal shear

$Q_0$	$a_1 : a_2 : a_3$	$\frac{a_3(t_c)}{a_2(t_c)}$
0	1: 1.25: 1.5	1.9
0.1	1: 1.25: 1.5	2.5
0.2	1: 1.25: 1.5	3.3
0.4	1: 1.25: 1.5	5.9
$Q_0$	$a_1 : a_2 : a_3$	$\frac{a_3(t_c)}{a_2(t_c)}$
0	1: 1.25: 1.7	2.8
0.1	1: 1.25: 1.7	3.7
0	1: 1.25: 2	4.6
0.1	1: 1.25: 2	6

*isolated* ellipsoid with  $a_1 : a_2 : a_3 = 1 : 1.25 : 1.7$ , I get  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 2.8$ . If the ellipsoid is *unisolated* ( $b = (-0.5, -0.5, 1)$ ,  $Q_0 = 0.1$ ), I get  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 3.7$ . The isolated ellipsoid with  $a_1 : a_2 : a_3 = 1 : 1.25 : 2$  gives  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 4.6$  while the *unisolated* ( $b = (-0.5, -0.5, 1)$ ,  $Q_0 = 0.1$ ) one gives  $\frac{a_3(t_c)}{a_2(t_c)} \simeq 6$ .

The previous one are only some examples (summarized in Table. 1) of how the model can be used to get information on the effect of external and internal shear on structures formation.

#### 4. Evolution of the axial peculiar velocity and of the density contrast

The approximate solution obtained in the previous section can be used to calculate the evolution of the axial peculiar velocity. I use Eqs. (20)-(22) to calculate the peculiar velocity along the axis of the ellipsoid in units of the Hubble expansion velocity,  $H$ :

$$\frac{v_i}{Ha_i} = \left| \frac{\dot{a}_i}{Ha_i} - 1 \right| \quad (31)$$

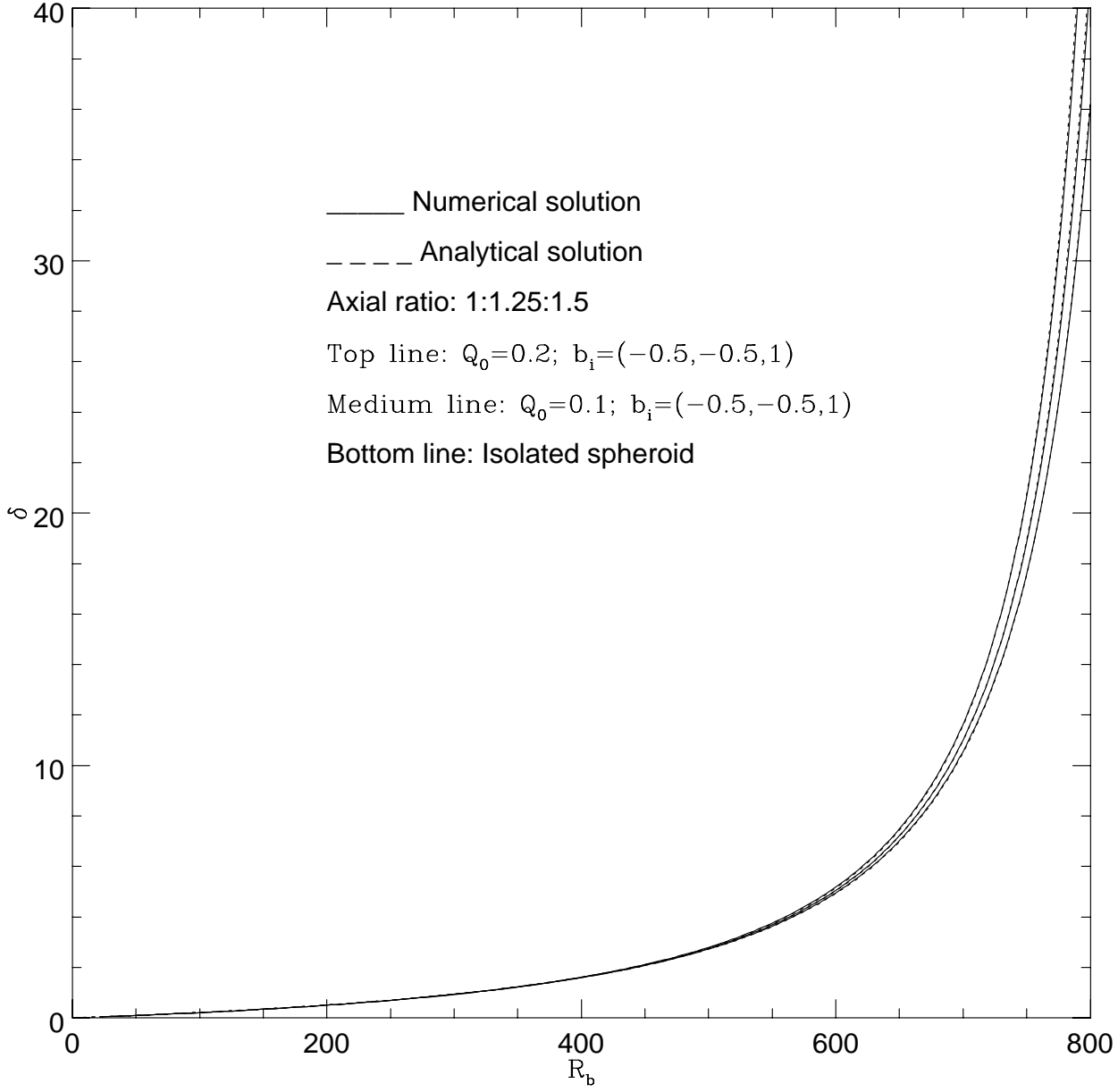
The results of the calculation are plotted in Figs. 3a-3e. In Figs. 3a-3c, I study how the internal shear influences the evolution of the velocity. In all three figures, the solid line represents, from up to bottom, the numerical result for the peculiar velocity along the shortest, medium and longest axis. The dotted line represents the velocity obtained from Eq. (31) using the approximation for the semiaxes (Eqs. (20)-(22)). Going from Fig. 3a to Fig. 3c, the value of  $Q_0$  is 0.1,  $b_i = (-0.5, -0.5, 1)$  and the axial ratio 1 : 1.25 : 1.5, 1 : 1.25 : 5, 1 : 2 : 3, respectively. For what concerns the goodness of the approximation, the plots show that the approximate solution is in good agreement with the numerical results. From the physical point of view, the plots show that there is a considerable difference between the peculiar velocities of the longest and shortest axes and in particular that the shorter is the axis the larger is the velocity of collapse.

The effect of the external field is shown in Figs. 3d-3e. The solid line in Fig. 3d represents the peculiar velocity for an ellipsoid of axial ratio 1 : 1.25 : 1.5 when no external field is present, while the dotted and dashed lines represent the case  $Q_0 = 0.1$ ,  $b_1 = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.2$ ,  $b_1 = (-0.5, -0.5, 1)$ , respectively. The situation is similar to that seen when I described the evolution of the semiaxes for different values of the external field. External shear produces different effects on the axes: the evolution of the longest axis, which is characterized by the smallest velocity, tend to be slowed down with increasing strength of the external field (dotted and dashed lines). The effect of external shear on the shortest and medium axes is opposite to that on the longest one, namely shear produce an acceleration in their evolution. Fig. 3e is the same as the previous one, but now the axial ratio is 1 : 2 : 3. Similarly to the previous plot, increasing the strength of the external field produce an acceleration of evolution in the shortest and medium axes and the opposite effect on the longest one. Another feature shown by a comparison of Fig. 3d and Fig. 3e is that the evolution of the shortest axis is accelerated with increasing asymmetry of the structure while the opposite is true for the longest axis: as noted before, external and internal shear have a qualitative similar effect on the evolution of the shortest and longest axes. The difference between the velocities along the longest and shortest axes is larger for *unisolated* ellipsoids than for the *isolated* ones and this difference increases with increasing strength of the external field.

The evolution of the density contrast can be calculated using the usual definition:

$$\delta = \frac{\rho_e - \rho_b}{\rho_b} = \frac{\rho_{e0}}{\rho_{b0}} \frac{a_{10}}{a_1} \frac{a_{20}}{a_2} \frac{a_{30}}{a_3} \left( \frac{R_b}{R_{b0}} \right)^3 - 1 \quad (32)$$

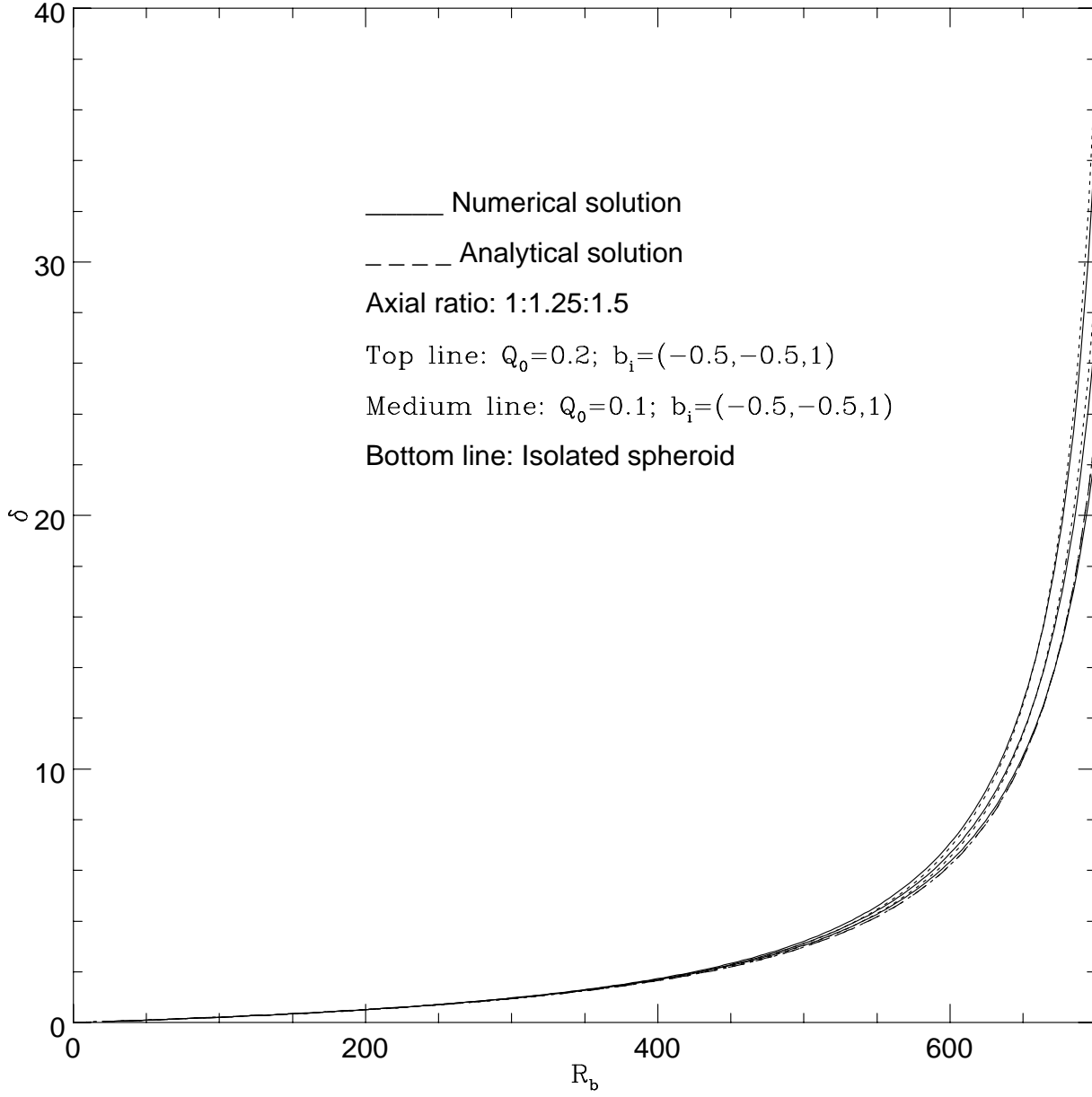
As for the peculiar velocity, I calculated the evolution of the density contrast of the ellipsoid both numerically and introducing the approximate analytical solution (Eqs. (20)-(22)) in Eq. ((32)). The result is plotted in Figs. 4a-4b. In both figures the solid lines represent the numerical results and the dotted lines the approximation, which is in good agreement with the numerical results. In Fig. 4a, the axial ratio of the ellipsoid is 1 : 1.25 : 1.5, the lines from bottom to top represent the case of an *isolated* ellipsoid ( $b_1 = (0, 0, 0)$ ),  $Q_0 = 0.1$ ,  $b_1 = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.2$ ,  $b_1 = (-0.5, -0.5, 1)$ , respectively. The plot shows that increasing the strength of the external field the value of the density contrast increases. Fig. 4b is the same of the previous one but the configuration is less spherical, with axial ratio 1 : 2 : 3. This last figure shows that more asymmetrical initial configurations tend to have, at a given time, larger values of  $\delta$ , which means that the collapse time decreases with increasing initial asymmetry. Then internal and external shear produce a more rapid evolution of the density contrast.



**Fig. 4a** The evolution of the density contrast. The axial ratio of the ellipsoid is 1 : 1.25 : 1.5, the lines from bottom to top represent the case of an *isolated* ellipsoid ( $b_i = (0, 0, 0)$ ),  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$ , and  $Q_0 = 0.2$ ,  $b_i = (-0.5, -0.5, 1)$ , respectively.

### 5. Overdensity at turnaround and velocity at collapse

As reviewed in the introduction, in literature there is not full agreement on the effect of shear on the collapse of density perturbations: while according to Bertschinger & Jain's (1994) collapse theorem the spherical perturbations are the slowest in collapsing, several other studies conclude in the opposite sense (Peebles & Groth 1976; Davis & Peebles



**Fig. 4b** Same of the previous one but the configuration is less spherical, with axial ratio 1 : 2 : 3.

1977; BS; Szalay & Silk 1983; Villumsen & Davis 1986; Peebles 1990; Bond & Myers 1993 a,b; Lokas et al. 1996; Audit et al. 1997).

In other words, the results concerning the effect of shear on collapse, are of two opposite kind:

1) Shear slows down the collapse (Peebles & Groth 1976; Davis & Peebles 1977; BS; Szalay & Silk 1983; Villumsen & Davis 1986; Peebles 1990; Bond & Myers 1993 a,b; Lokas et al. 1996; Audit et al. 1997). This result is obtained, for example, if one uses

homogeneous ellipsoids to model an *extended* mass distribution and not vanishing mass elements and collapse is followed even after the collapse of the first axis: the collapse of one axis is 'frozen' when it becomes smaller than a certain value, and the collapse of the other axes is followed till the collapse of the third axis, which defines the collapse time. This is done to simulate the virialization process. In fact, as remarked by Eisenstein and Loeb (1995), after the short axis collapses, it makes a small contribution to the quadrupole moment of the ellipsoid (the reason is due to the fact that the quadrupoles are proportional to the difference between the squares of the lengths of the axes) and then, in order to take into account the acquisition of angular momentum rightly, it is necessary to follow the collapse after the first axis collapse.

2) Shear accelerates the collapse (e.g., Hoffmann 1986a, 1989; Evrard & Crone (1992), Bertschinger & Jain (1994)). This result is obtained in papers dealing with the evolution of individual mass elements for which the collapse correspond to the collapse of the first axis.

In the following of this section, I shall show that, even if the effects of substructure are neglected, by approximating the structure formation by means of an homogeneous ellipsoid, and even if one assumes that the collapse is stopped when the first axis collapses, the shear slows down the rate of growth of the density contrast by lowering the peculiar velocity (WS; BS; Szalay & Silk 1983).

To this aim, in the following, I re-derive the fundamental equations in BS for an homogeneous ellipsoid model taking also into account the external field (in BS, only the collapse of an *isolated* ellipsoid model was studied). These equations shall be used to study the velocity at collapse and the overdensity at turnaround.

The evolution of the ellipsoid can be obtained using Eqs. (20-22):

$$x(t) = R_b - \frac{3}{2}\tilde{\alpha}_1 (R_b - R_e) - d \times R_b^{\left(\frac{2+3c_1}{2}\right)} \left(1 - \frac{3\tilde{\alpha}_1}{2}\right) \quad (33)$$

$$y(t) = R_b - \frac{3}{2}\tilde{\alpha}_2 (R_b - R_e) \quad (34)$$

$$z(t) = R_b - \frac{3}{2}\tilde{\alpha}_3 (R_b - R_e) \quad (35)$$

Using BS notation, I indicate with  $x(t) = x_o X(t)$ ,  $y(t) = y_o Y(t)$  and  $z(t) = z_o Z(t)$ , the principal axes ( $x_o$ ,  $y_o$  and  $z_o$  are the initial values of the axes). The overdensity of the ellipsoid is the same used till now, the initial conditions are  $X = Y = Z = R_b = R_e = 1$  at  $t = t_0$  and as before the initial velocity is equal to the Hubble velocity at  $t_0$  (representing the initial time). The parametric equations satisfied by  $R_e(t)$  are:

$$R_e = \frac{1}{2\delta} (1 - \cos(\vartheta)), \quad \frac{t}{t_0} = \frac{3}{4\delta^{3/2}} (\vartheta - \sin(\vartheta)) \quad (36)$$

while, since our background is an EdS universe,  $R_b(t) \propto t^{2/3}$ .

Following BS, it is easy to find that the density contrast is given by:

$$\delta_i = \frac{R_b^3}{XYZ} - 1 = f_1^2(\vartheta) \left[ \left(1 - \frac{3\tilde{\alpha}_1}{2}\right) f_1^{\frac{2}{3}}(\vartheta) + \frac{3}{4}\tilde{\alpha}_1 f_2(\vartheta) - d \left(1 - \frac{3\tilde{\alpha}_1}{2}\right) \frac{f_1^{\frac{2f}{3}}(\vartheta)}{\delta^{f-1}} \right]^{-1} \times \\ \left[ \left(1 - \frac{3\tilde{\alpha}_2}{2}\right) f_1^{\frac{2}{3}}(\vartheta) + \frac{3}{4}\tilde{\alpha}_2 f_2(\vartheta) \right]^{-1} \left[ \left(1 - \frac{3\tilde{\alpha}_3}{2}\right) f_1^{\frac{2}{3}}(\vartheta) + \frac{3}{4}\tilde{\alpha}_3 f_2(\vartheta) \right]^{-1} - 1 \quad (37)$$

where  $f = \frac{2+3c_1}{2}$ ,  $f_1(\vartheta) = \frac{3}{4}(\vartheta - \sin(\vartheta))$  and  $f_2(\vartheta) = 1 - \cos(\vartheta)$ . The density contrast at turn-around is obtained by calculating  $\delta_i(\vartheta_{\text{ta}})$ , where the parameter  $\vartheta$  at turnaround epoch is given solving the equation:

$$\frac{2}{3\tilde{\alpha}_1} = \frac{df R_b^{f-1} + \frac{\sin(\vartheta_{\text{ta}})}{f_2(\vartheta_{\text{ta}})} f_1^{\frac{1}{3}} - 1}{df R_b^{f-1} - 1} \quad (38)$$

Eqs. (37), (38) reduces to BS Eqs. (76) and (72) for  $d = 0$ ,  $\tilde{\alpha}_1 = \alpha_1$ ,  $\tilde{\alpha}_2 = \alpha_2$ ,  $\tilde{\alpha}_3 = \alpha_3$ .

<sup>3</sup> Eq. (37) yields the familiar value  $\delta = (3\pi/4)^2$  in the spherical case, ( $d = 0$ ,  $\tilde{\alpha}_1 = \alpha_1 = \tilde{\alpha}_2 = \alpha_2 = \tilde{\alpha}_3 = \alpha_3 = 2/3$ ). In general, in order to obtain the density contrast at turnaround, one has first to solve Eq. (38) for  $\vartheta$  for an arbitrary axial ratio and substitute the value in Eq. (37). The time of turn-around can be calculated by means of:

$$t = \frac{3t_0}{4\delta^{3/2}}(\vartheta - \sin(\vartheta)) = \frac{t_{\text{ff}}}{2\pi}(\vartheta - \sin(\vartheta)) \quad (39)$$

where  $t_{\text{ff}}$  is the free-fall time:

$$t_{\text{ff}} = \frac{3\pi}{2\delta^{3/2}} t_0 \quad (40)$$

In Fig. 5, I plotted the density contrast at turn-around for a prolate spheroid for several values of the longest axis,  $a_3$ , (the other two axes have fixed value  $a_1 : a_2 = 1 : 1$ ) (note that from now on, and in the figures,  $a_i$  represents the initial value of the  $i$ -th axis). The solid lines, from top to bottom, represent numerical results for the density contrast for an *isolated* spheroid ( $b_i = (0, 0, 0)$ ), and for *unisolated* spheroids with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and  $Q_0 = 0.2$ ,  $(-0.5, -0.5, 1)$ , respectively. The dashed lines represent the approximate solution (Eq. (37)). The figure shows that the density contrast at turn-around is reduced, relative to the value  $\delta = (3\pi/4)^2$  typical of spherical collapse when  $a_3 > 1$ . This reduction increases with increasing initial asymmetry of the spheroid. Although not shown, the reduction is larger for oblate spheroids: in this case, for extreme initial flattening (8:8:1) the value of  $\delta_{\text{ta}}$  can be reduced to values as small as  $\simeq 1$ . The effect of the external field is that of reducing the value of  $\delta_{\text{ta}}$  even more. An interesting question that can arise because of the previous result is the following: if at turn-around the density contrast predicted by the ellipsoid model can be a factor 3 smaller than that of the spherical model, then one should expect that the difference

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<sup>3</sup> In reality some equations in BS contains some typographical misprints, for example this is the case of Eq. (76) and Eq. (80).



between the two model starts at  $\delta < (3\pi/4)^2$ . Does the prediction of these two models match in the linear theory? In order to answer this question, I compared the value of  $\delta$  given by the ellipsoid model to that of the spherical one. The result is plotted in Fig. 6. The solid line represents the density contrast predicted by the spherical model, while the dotted, short-dashed, long-dashed and long-dashed-short-dashed lines represents the prediction of the ellipsoid model with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and initial axial ratio  $1 : 1.25 : 1.5$ ,  $1 : 1.25 : 3$ ,  $1 : 1.25 : 5$ ,  $1 : 1.25 : 8$ , respectively. As shown, the difference between the prediction of spherical and ellipsoid model starts at  $\delta > 1$ . In Fig. 7, the same calculation is repeated for an oblate spheroid. Here, the solid line represents the density contrast predicted by the spherical model, while the dotted, short-dashed, long-dashed lines represents the prediction of the model with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and initial axial ratio  $2 : 2 : 1$ ,  $4 : 4 : 1$ ,  $8 : 8 : 1$ , respectively. In this case the two models start to give different predictions at  $\delta \simeq 0.6$ . So in both cases, the two models are different only when we are far away from the linear regime.

The density contrast at virialization is a bit more difficult to calculate. To begin with, it is important to recall the difference between virialization and collapse: this last term describe a state of the system in which the density approaches infinity, while virialization is characterized by  $|U| = 2K$ , where  $U$  and  $K$  are, respectively, the potential and kinetic energy. Only in the case of perfectly spherical infall, collapse and virialization are synonymous (although in the case of a bound system one follows rapidly the other). In this case, the infall cannot be halted and it proceeds towards a singularity, with all mass of the system collapsing to a single point which means that the density contrast becomes infinite. This result is physically unacceptable and to prevent the system to reach this state it is necessary to introduce, by hand, the assumption that the collapse halts when spherical shells reach a particular radius  $r_f = r_v = r_{ta}/2$ , (where  $r_f$ ,  $r_v$  and  $r_{ta}$  are the final radius, the virialization radius and the turnaround radius, respectively).<sup>4</sup> Then, in the spherical infall model, the density contrast of the virializing structure is calculated assuming that, after the shell collapses, the final radius is  $r_f = r_v = r_{ta}/2$ : this leads to the conclusion that  $\delta_v = 178$ . The density contrast of a non-spherical virialized system can be calculated using the same definition given for the spherical system, namely:

$$\delta_v = \frac{R_b^3(t_c)}{X(t_{1/2})Y(t_{1/2})Z(t_{1/2})} - 1 \quad (41)$$

where  $t_{1/2}$  is the time at which the shortest axis has a length  $1/2$  of the value at maximum expansion,  $x(t_{1/2}) = x_{ta}/2$  (see Peebles 1990).

The time at collapse of the shortest axis can be obtained by means of the second of Eq. (36) once the parameter  $\vartheta_c$  at the collapse time, characterized by  $X(t_c) = 0$ , is

<sup>4</sup> This major drawback of the spherical model is removed by taking account of the angular momentum in the equation of motion (see Engineer et al. 2000).

known. After some calculations it is possible to show that  $\vartheta_c$  can be obtained solving the following equation:

$$\frac{2}{3\tilde{\alpha}_1} = \frac{\frac{1-\cos(\vartheta_c)}{2} f_1^{-\frac{2}{3}}(\vartheta_c) + d \left( \frac{f_1^{\frac{2}{3}}(\vartheta_c)}{\delta} \right)^{f-1} - 1}{d \left( \frac{f_1^{\frac{2}{3}}(\vartheta_c)}{\delta} \right)^{f-1} - 1} \quad (42)$$

which, for  $d = 0$  and  $\tilde{\alpha}_1 = \alpha_1$ , reduces to Eq. (78) of BS. The time  $t_{1/2}$ , or equivalently,  $\vartheta_{1/2}$ , is obtained solving the equation:

$$x(t_{1/2}) = x_{\text{ta}}/2 \quad (43)$$

where  $x(t)$  is given in Eq. (33) and  $x_{\text{ta}}$  is obtained using again Eq. (33) and calculating  $x(\vartheta_{\text{ta}})$ . The result is plotted in Fig. 8. The solid line shows that, with increasing initial anisotropy, the density contrast decreases from the value  $\delta_v = 178$ , for the spherical case, to a value of  $\delta_v \simeq 48$ , for large initial 'flattening' (semiaxes ratio 1:1:8). The result plotted refers to an *isolated* prolate spheroid, while for the oblate case and for the same axial ratio (8:8:1) results  $\delta_v \simeq 11$ . These results are in qualitative agreement with Peebles (1990).

The results in Figs. 5-8 could seem in disagreement with Fig. 4a-4b, since in those figures the value of  $\delta$  increases with increasing initial asymmetry of the ellipsoid. The reason why  $\delta_{\text{ta}}$  decreases with increasing initial asymmetry is due to the fact that the turn-around  $t_{\text{ta}}$ , and also the collapse epoch, moves towards lower values of time,  $t$ , for larger values of initial asymmetry of a given perturbation and larger strength of the external field. This last effect is shown in Fig. 9: the solid, short-dashed and long-dashed lines, represent respectively the time of turn-around for an *isolated* spheroid and for spheroids having  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and  $Q_0 = 0.2$ ,  $(-0.5, -0.5, 1)$ . More asymmetric structures are characterized by a smaller value of turn-around time, and the external field contributes to this reduction of  $t_{\text{ta}}$ . In the case of oblate spheroids, the collapse time can be reduced to values  $t \simeq 0.3t_{\text{ff}}$  for initial axial ratio 8 : 8 : 1.

Another interesting quantity that can be obtained is the collapse velocity at the time of collapse. I shall calculate the collapse velocity using the same steps followed by BS, with the difference that the spheroids considered in the following are prolate. Their evolution is obtained as before, putting Eqs. (33-35) in the equation for the collapse velocity down the shortest axis:

$$v_x = x_0 \dot{X} \quad (44)$$

Calculating the derivative of Eq. (33) and inserting it in Eq. (44), I find that:

$$v_{\text{xc}} = -x_0 \frac{3}{2} \tilde{\alpha}_1 \dot{R}_b \left[ 1 - \frac{2}{3\tilde{\alpha}_1} - \left( \frac{3}{4} \right)^{\frac{1}{3}} \frac{\sin(\vartheta_c) (\vartheta_c - \sin(\vartheta_c))}{1 - \cos(\vartheta_c)} + df R_b^{f-1} \left( \frac{2}{3\tilde{\alpha}_1} - 1 \right) \right] \quad (45)$$

here the subscript “c” means that the corresponding quantity is calculated at the collapse epoch. Eq. (45) can be written in a different form using the following equations:

$$Z_c = R_{bc} - \frac{3\tilde{\alpha}_3}{2} (R_{bc} - R_{ec}) = R_{bc} \left( 1 - \frac{\tilde{\alpha}_3}{\tilde{\alpha}_1} \right) + \frac{3\tilde{\alpha}_3}{2} d \left( \frac{2}{3\tilde{\alpha}_1} - 1 \right) R_b^f \simeq R_{bc} \left( 1 - \frac{\tilde{\alpha}_3}{\tilde{\alpha}_1} \right) \quad (46)$$

(see Eq. (79) of BS). Approximating Eq. (42) by means of Eq. (78) of BS:

$$1 - \frac{2}{3\tilde{\alpha}_1} = \frac{1 - \cos(\vartheta_c)}{2} \left[ \frac{3}{4} (\vartheta_c - \sin(\vartheta_c)) \right]^{\frac{-2}{3}} \quad (47)$$

and approximating the equation  $x = 0$ , defining the collapse time, with the Eq. (77) of BS:

$$(1 - \cos(\vartheta_c)) / 2\delta = R_{bc} \left( 1 - \frac{2}{3\alpha_1} \right) \quad (48)$$

Finally I get:

$$v_{xc} = - \left[ \frac{\dot{R}_{bc}}{R_{bc}} r_c \right] \frac{3\tilde{\alpha}_1 - 2}{\tilde{\alpha}_1 - \tilde{\alpha}_3} \left\{ 1 - \frac{3 \sin(\vartheta_c) (\vartheta_c - \sin(\vartheta_c))}{2 (1 - \cos(\vartheta_c))^2} + \right. \\ \left. 2df \left[ \frac{1 - \cos(\vartheta_c)}{2\delta \left( 1 - \frac{2}{3\tilde{\alpha}_1} \right)} \right]^{f-1} \left( \frac{2}{3\tilde{\alpha}_1} - 1 \right) \frac{\left[ \frac{3}{4} (\vartheta_c - \sin(\vartheta_c)) \right]^{\frac{2}{3}}}{1 - \cos(\vartheta_c)} \right\} \frac{x_0}{z_0} \tilde{\alpha}_1 \quad (49)$$

where  $r_c = z_0 Z_c$  is the radius of the collapsed object and  $R_{bc}$  represents  $R_b(t_c)$ . Using Eq. (49) instead of Eq. (45) introduces errors of order  $\simeq 10\%$ . In the case of a prolate spheroid, one has that:

$$v_{xc} = - \left[ \frac{\dot{R}_{bc}}{R_{bc}} r_c \right] \frac{3\tilde{\alpha}_1 - 2}{\tilde{\alpha}_1 - \tilde{\alpha}_3} \left\{ 1 - \frac{3 \sin(\vartheta_c) (\vartheta_c - \sin(\vartheta_c))}{2 (1 - \cos(\vartheta_c))^2} + \right. \\ \left. 2df \left[ \frac{1 - \cos(\vartheta_c)}{2\delta \left( 1 - \frac{2}{3\tilde{\alpha}_1} \right)} \right]^{f-1} \left( \frac{2}{3\tilde{\alpha}_1} - 1 \right) \frac{\left[ \frac{3}{4} (\vartheta_c - \sin(\vartheta_c)) \right]^{\frac{2}{3}}}{1 - \cos(\vartheta_c)} \right\} \sqrt{1 - e^2} \tilde{\alpha}_1 \quad (50)$$

where I have defined  $1 - e^2 = (x_0/z_0)^2$ . In the case of an oblate spheroid:

$$v_{zc} = - \left[ \frac{\dot{R}_{bc}}{R_{bc}} r_c \right] \frac{3\tilde{\alpha}_3 - 2}{\tilde{\alpha}_3 - \tilde{\alpha}_1} \left\{ 1 - \frac{3 \sin(\vartheta_c) (\vartheta_c - \sin(\vartheta_c))}{2 (1 - \cos(\vartheta_c))^2} + \right. \\ \left. 2df \left[ \frac{1 - \cos(\vartheta_c)}{2\delta \left( 1 - \frac{2}{3\tilde{\alpha}_3} \right)} \right]^{f-1} \left( \frac{2}{3\tilde{\alpha}_3} - 1 \right) \frac{\left[ \frac{3}{4} (\vartheta_c - \sin(\vartheta_c)) \right]^{\frac{2}{3}}}{1 - \cos(\vartheta_c)} \right\} \sqrt{1 - e^2} \tilde{\alpha}_3 \quad (51)$$

having defined  $1 - e^2 = (z_0/x_0)^2$  and  $r_c = x_0 X_c$ . If  $d = 0$ ,  $\tilde{\alpha}_1 = \alpha_1 = \tilde{\alpha}_2 = \alpha_2 = \tilde{\alpha}_3 = \alpha_3 = 2/3$ , the spheroid is isolated and Eq. (82)-(83) of BS is recovered.

In Fig. 10, I plot  $\frac{v_{xc}}{H_c r_c}$ , as a function of the ratio of the initial value of the axes,  $a_3/a_1$ . The solid lines represent numerical results of the collapse velocity for a prolate spheroid ( $a_1 = a_2 < a_3$ ), the dotted lines represent the result obtained from the approximate solution. The top curve represents the velocity for an *isolated* spheroid, the medium one the same quantity for a spheroid having  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$ , and the last bottom curve the velocity for a spheroid having  $Q_0 = 0.2$ ,  $b_i = (-0.5, -0.5, 1)$ .

The figure shows two trends:

- a) the collapse velocity is reduced with increasing initial asymmetry. For example for  $a_1/a_3 = 0.3$  the collapse velocity is reduced to the Hubble velocity in the plane of collapse (plane of the pancake for oblate spheroids) ( $H_c r_c$ ), while in the case of more extreme 'flattening'  $a_1/a_3 = 0.125$ , the collapse velocity is reduced by a factor of  $\simeq 2.5$  with respect the previous value. In the case of oblate spheroids, for this last initial asymmetry, this value is  $\simeq 6$ .
- b) The collapse velocity is reduced with increasing strength of the external field. In the case of the bottom curve, for  $a_1/a_3 = 0.125$ , the collapse velocity is reduced by a factor of  $\simeq 3$ . Similarly to item (a), in the case of oblate spheroids, for this last initial asymmetry, this value can be larger than  $\simeq 6$ .

In other words, the slowing down of the rate of growth of density contrast produces a lowering of the peculiar velocity in qualitative and quantitative agreement with BS and Szalay & Silk (1983).

The results obtained help to clarify the controversy relative to the previrialization conjecture. According to this paper and with WS and BS and in agreement with Hoffman (1986a) and Bertschinger & Jain's collapse theorem, it is surely true that the effect of the shear is to reduce the collapse time of perturbations. As remarked in the item "b" of section (3) and in agreement with WS and BS: *The collapse time of perturbations of fixed initial overdensity, for a fixed background, decreases with increasing initial asymmetry.* The decrease of the collapse time has such entity to compensate the effect of the increase of density contrast and collapse velocity produced by the shear. To be more clear, it is useful to concentrate on Figs. 3-4. If the collapse of the ellipsoids occurred at a fixed value of  $t$ , just like for the spherical model ( $t = 0.5t_{ff}$ ), the larger increase in density contrast or velocity produced by the initial asymmetry, in comparison with the spherical model, should have as a result that at collapse both the density contrast and velocity should be enhanced (with respect to the spherical model). But in the ellipsoidal collapse, the collapse time decreases with increasing initial anisotropy, and as we have previously seen, in case of initial axial ratio  $8 : 8 : 1$  it is given by  $t \simeq 0.3t_{ff}$ . As a consequence, the values of density contrast and collapse velocity at collapse time are always reduced with respect the spherical collapse, in agreement with WS, BS, Szalay & Silk (1983).

I must also add that in the real collapse other effects have an important role, (e.g., the effects of small scale substructure). Both Hoffman (1986a) and Bertschinger & Jain (1994) results are valid for a fluid element, which has no substructure by definition, while a small scale substructure produces a slowing down of the collapse at least in two ways: 1) encounters between infalling clumps and substructure internal to the perturbation (Antonuccio-Delogu & Colafrancesco 1994; Del Popolo & Gambera 1997; Del Popolo &

Gambera 1999);

2) tidal interaction of the main proto-structure with substructure external to the perturbation (Peebles 1990; Del Popolo & Gambera 1998).

Moreover, it should be pointed out that, as more small-scale power is present, the collapse of a perturbation may be slowed down in a way that could inhibit the effect of shear.

Similarly to Bertschinger & Jain (1994), the model presented in this paper does not take account of the substructure internal to the system. I, however, recall that the same shortcoming was present in Peebles (1990): in that paper the substructure was suppressed, since it adopted an homogeneous Poisson distribution of particles within the protocluster (Peebles 1990). This limit has the effect of underestimating the effect of previrialization, (Peebles 1990). In other words, the slowing down of the collapse obtained in this paper (similarly to that of Peebles (1990)) are surely smaller than that we shall find if we had used a system having internal substructure, as in the above point 1.

Before concluding, I want to spend a few words on the impact of the result of the paper on our view of structure formation.

The reduction of the rate of growth of overdensity and collapse velocity has several consequences on structure formation. To begin with, a first consequence is a change of the mass function, the two-point correlation function, and the mass that accretes on density peaks. These last consequences are connected to the effects of the shear (Audit, Teyssier & Alimi 1997, 1998). According to Audit, Teyssier & Alimi (1997, 1998), the mass function depends on two parameters, a density threshold  $\delta_c$  and a shear threshold  $\sigma_c$ . According to the previous authors, structures results from a collapse along their third principal axis, which is slowed down by the effect of the shear (in agreement with our results). Therefore on small scales, where the shear is statistically greater, structures need on average a higher density contrast to collapse and as a consequence the number of objects with  $\sigma(M) \leq 1$ <sup>5</sup>, decrease as compared to the collapse of the second or first axis, and so the mass function is much below the standard Press-Schechter prediction. Even the two-point correlation function of galaxies and clusters of galaxies results strongly modified since the two-point correlation function of the collapsed halos is directly connected to the number of objects of a given mass (see Peebles 1993; Sheth & Jain 1997; Del Popolo & Gambera 1999; Del Popolo et al. 1999). Another important consequence of the results described is connected to the value of the density parameter,  $\Omega$ . Since the initial anisotropy (internal shear) and the tidal interaction with external objects (external shear), slow down the collapse infalling velocity, when using the spherical infall model we underestimate the value of the density parameter (Szalay & Silk 1983; Lee et al. 1986; Taruya & Soda 2000). The previous described effects are even larger if the structure acquires angular momentum

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<sup>5</sup>  $\sigma(M)$  is the mass variance

during evolution (Del Popolo & Gambera 1999; Del Popolo & Gambera 2000). In our model, we assumed that the principal axes of the external tidal tensor are always oriented along the principal axes of the mass tensor and this implies that the linear angular momentum should be zero (at least from the linear phase to shell-crossing), and so while it is legitimate to speak about the effects of shear on structure formation, we do not take account of the effects of angular momentum acquisition on structure formation, at least before gravitational collapse.<sup>6</sup> As a result, since tidal forces produces effects similar to that due to shear, the quoted limit has the consequence of underestimating the global effect on structure formation of the interaction of a protostructure with the neighboring ones (see also Del Popolo & Gambera 1999; Del Popolo & Gambera 2000).

Finally, we want to recall, as previously reported, that in the case of an initial spherical configuration our model reduces to Watanabe's. In this case, the misalignment condition is verified and the sphere can acquire angular momentum.

## 6. Conclusions

I examined the effect of internal and external shear on the evolution of non-spherical inhomogeneities in a EdS universe. The study was based upon an approximate analytical solution of the equation of motions of the axes of the ellipsoid. In the first part of the paper, I found the analytical solution to the quoted equations and I compared the result with the numerical solution of Icke (1973) equations, and in the case of *isolated* ellipsoids with the WS analytical solution. The analytical approximation is in good agreement with the numerical results both for *isolated* and *unisolated* ellipsoids, and it gives a better approximation to numerical results with respect to WS analytical solution. The quoted solution was used to study the effect of shear on the density contrast and peculiar velocity. The results show that:

a) The collapse time of perturbations of fixed initial overdensity, for a fixed background, decreases with increasing initial asymmetry and strength of the external field. To be more precise, the evolution of the shortest axis is accelerated with increasing asymmetry of the structure while the opposite is true for the longest axis. The effect of a positive tidal force, along a given axis, is that of slowing down the expansion of the ellipsoid along this axis and the effect of a negative tidal field is that of accelerating the expansion of the ellipsoid along that axis: external and internal shear have a qualitative similar effect on

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<sup>6</sup> However, since the collapse of a protostructure is a violent phenomenon, the conditions of Kelvin's circulation theorem should be violated (Chernin 1970). This leads to the acquisition of vorticity by the formation of shock fronts in the protostructure (pancake), in correspondence of shell-crossing (Doroshkevich 1970). Analytical studies by Pichon & Bernardeau (1999) have also shown that vorticity generation becomes significant at the scales  $3 - 4h^{-1}\text{Mpc}$ , and increases with decreasing scale.

the evolution of the shortest and longest axes.

b) The difference between the velocities along the longest and shortest axes is larger for *unisolated* ellipsoids than for the *isolated* ones and this difference increases with increasing strength of the external field.

c) While for *isolated* ellipsoids or for *unisolated* ones with small values of  $|\gamma|$ , the axial ratio does not appreciably change until the perturbation enters a strongly nonlinear regime, (the self-gravity is dominant), for large values of  $|\gamma|$ , the collapse is anisotropic even for not large values of  $\delta$ . This means that the collapsing region geometry is strongly influenced by the external shear: if the external field is strong enough, then external shear is dominant (with respect to internal shear) in shaping the region, in agreement with Eisenstein & Loeb (1995), Watanabe(1993).

d) Increasing the strength of the external field, the value of the density contrast increases.

e) More asymmetrical initial configurations tend to have, at a given time, larger values of  $\delta$ . Then internal and external shear produce a more rapid evolution of the density contrast.

In order to study the effect of shear on the density contrast at turnaround and velocity at collapse, I re derived the equations of the density contrast at turn-around and the velocity at collapse time of BS model, taking account of both internal and external shear. The results have shown that:

(aa) The values of density contrast and collapse velocity at collapse time are always reduced with respect the spherical collapse, in agreement with WS, BS, Szalay & Silk (1983).

(bb) The effects of the slowing down of the collapse obtained in this paper (similarly to that of Peebles (1990)) are surely smaller than that we would find if we had used a system having internal substructure.

(cc) The shear has a big impact on our view of structure formation:

(cc1) a first consequence is a change of the mass function, the two-point correlation function, and the mass that accretes on density peaks (see also Del Popolo & Gambera 2000; Audit et al. 1997; Del Popolo & Gambera 1999; Del Popolo et al. 1999; Peebles 1993).

(cc2) Another important consequence of the results described is connected to the value of the density parameter,  $\Omega$ . When using the spherical infall model we underestimate the value of the density parameter (Szalay & Silk 1983; Lee et al. 1986; Taruya & Soda 2000), since shear slows down the collapse infalling velocity.

Almost all the results obtained with the analytical model were tested against numerical solutions finding always good agreement with them.

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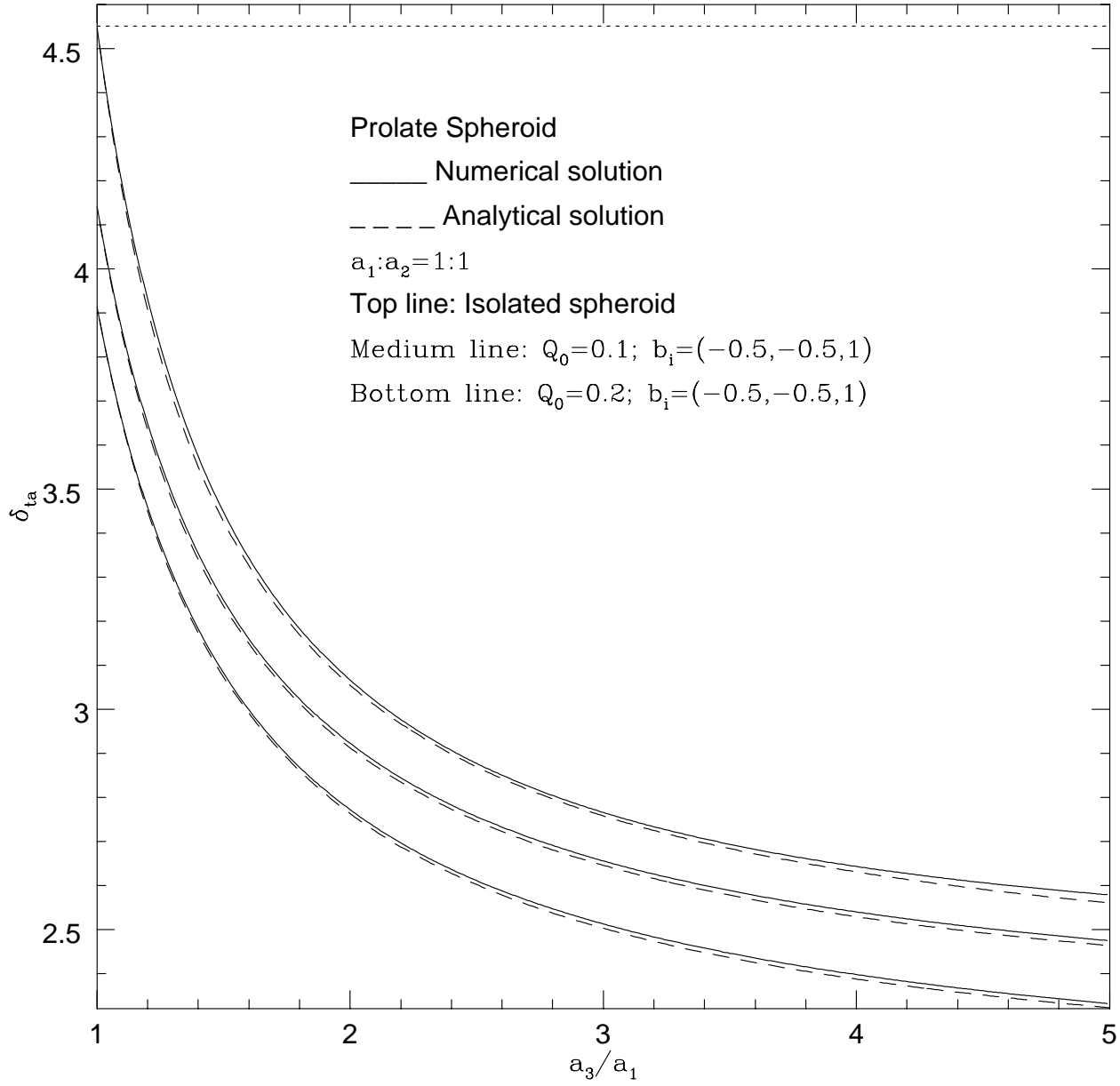
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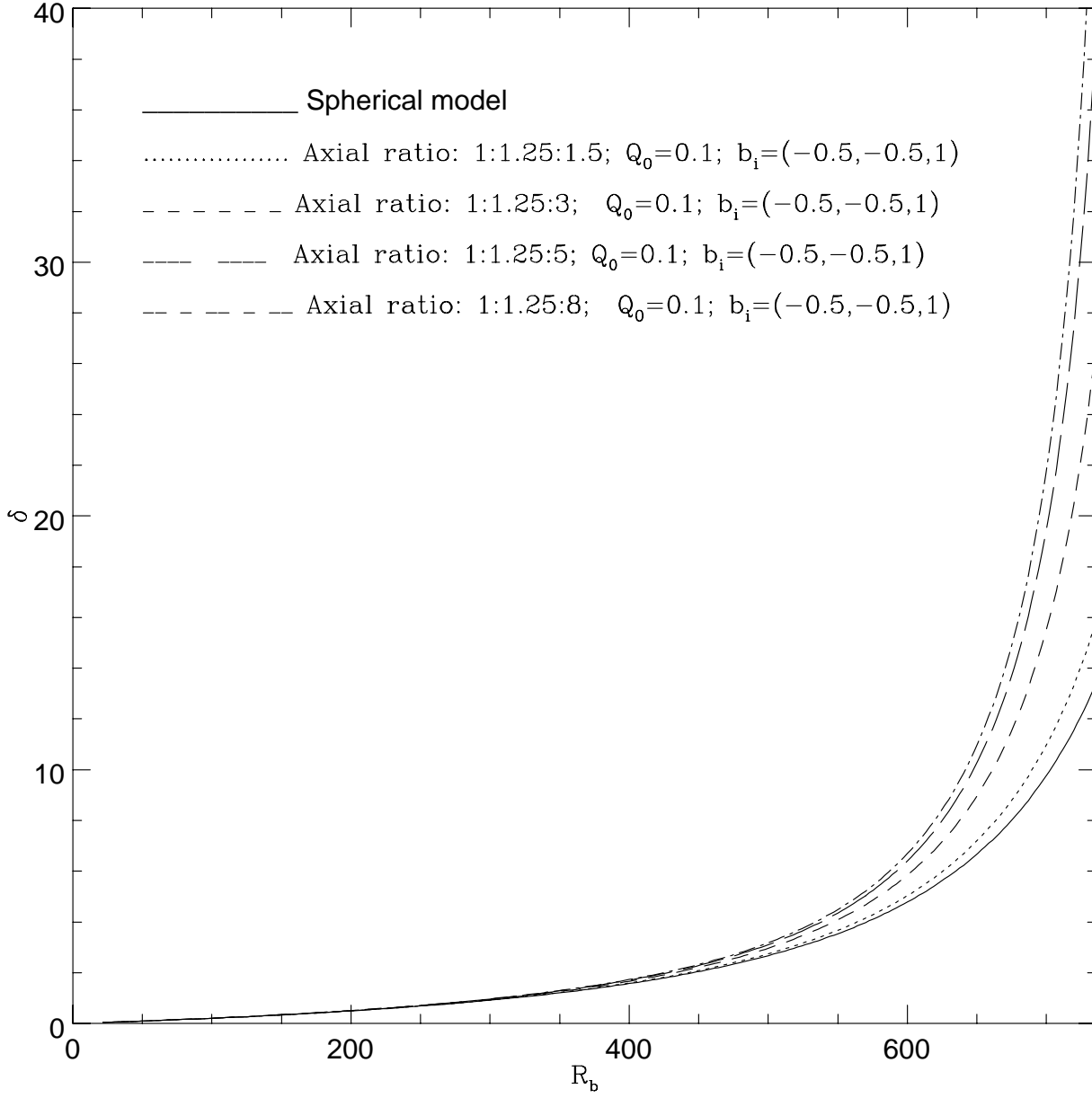
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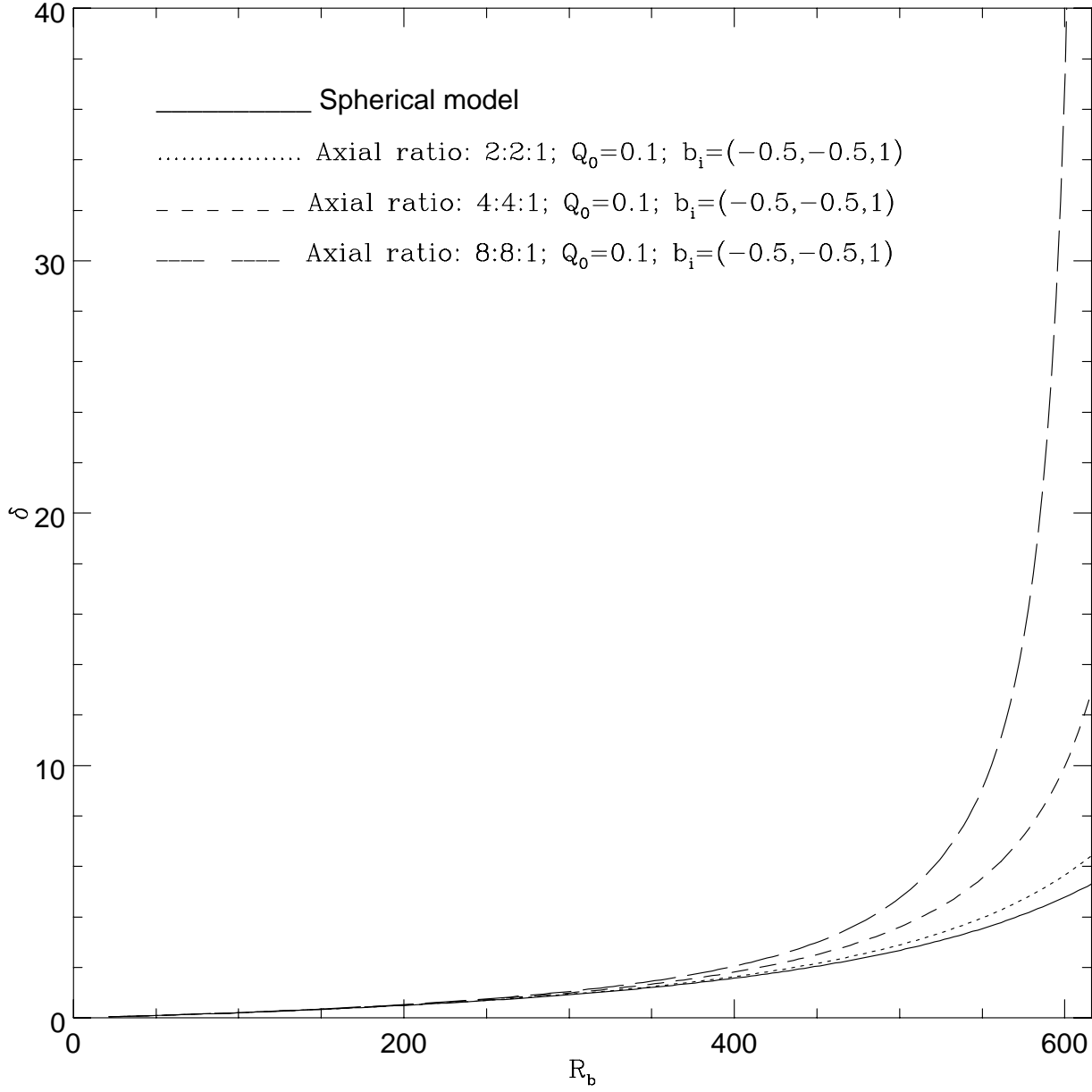
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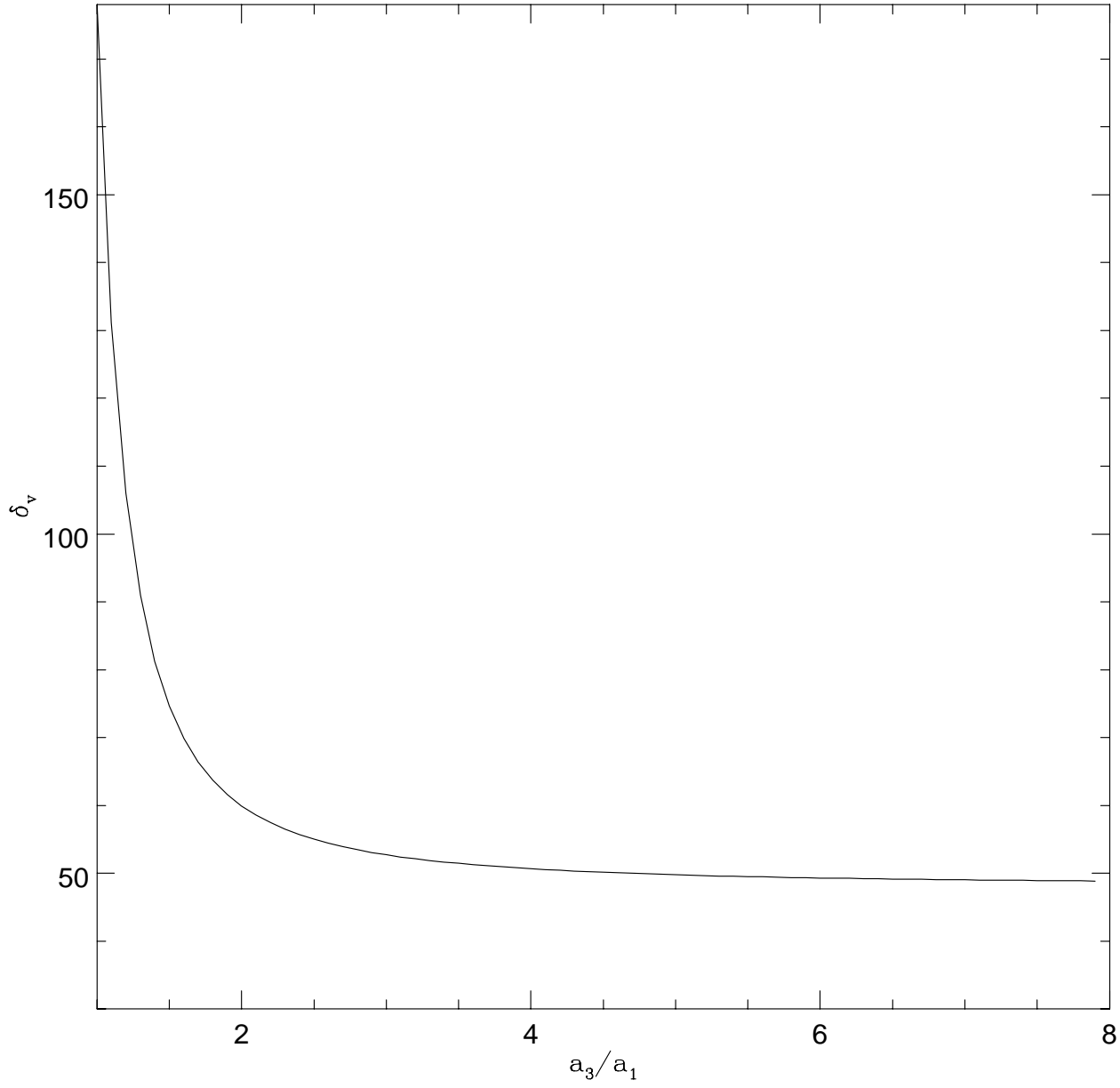
**Fig. 5** The density contrast at turnaround for a prolate spheroid for several values of the longest axis,  $a_3$ , (the other two axes have fixed value  $a_1 : a_2 = 1 : 1$ ). The solid lines, from top to bottom, represent numerical results for the density contrast for an *isolated* spheroid ( $b_i = (0, 0, 0)$ ), and for *unisolated* spheroids with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and  $Q_0 = 0.2$ ,  $(-0.5, -0.5, 1)$ , respectively. The dashed lines represent the approximate solution (Eq. (37)). The upper dotted line represents the value of the density contrast at turnaround for a spherical perturbation.



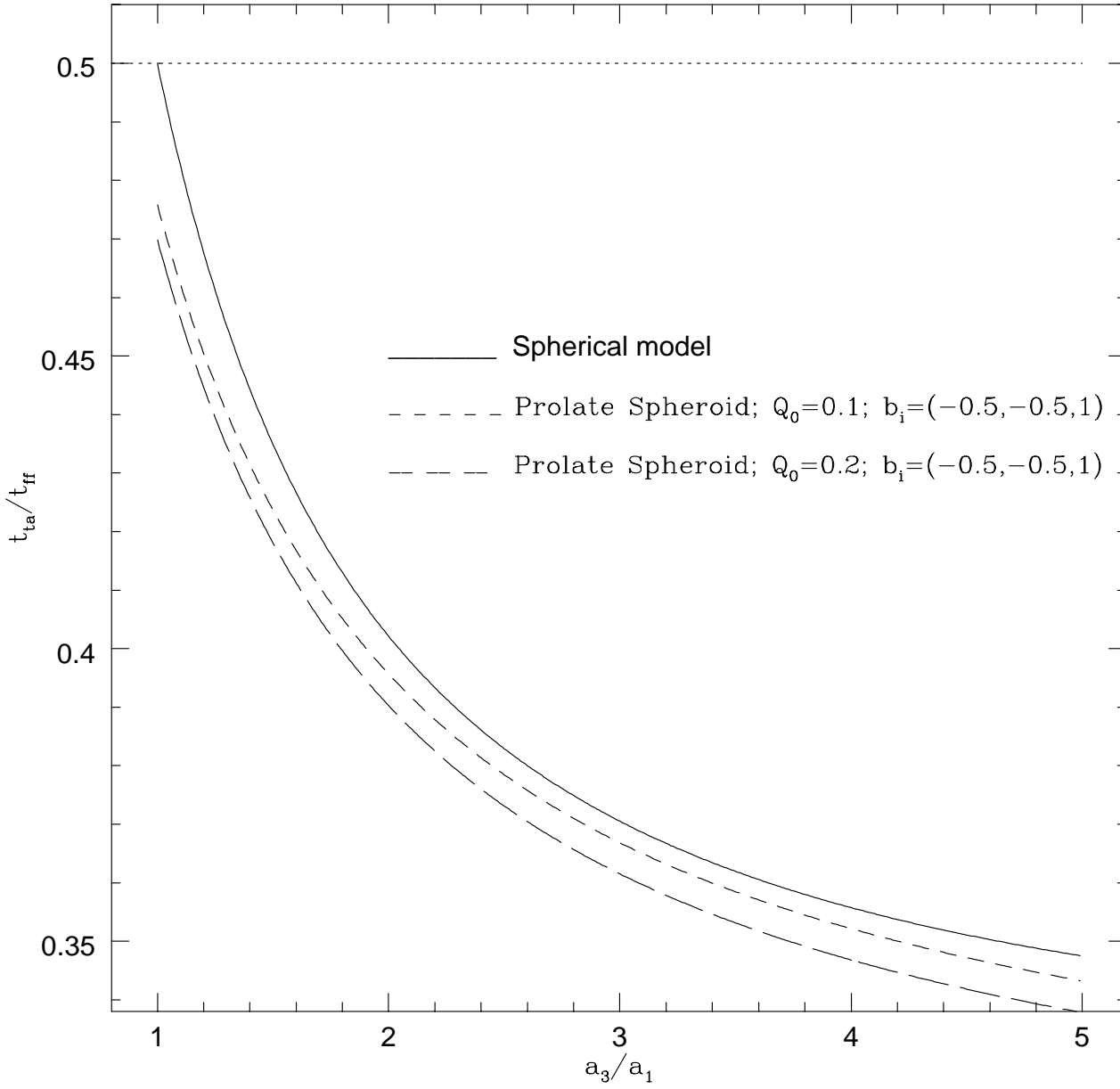
**Fig. 6** Comparison between density contrast predicted by spherical and ellipsoidal model. The solid line represents the density contrast predicted by the spherical model, while the dotted, short-dashed, long-dashed and long-dashed-short-dashed lines represents the prediction of the ellipsoid model with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and initial axial ratio 1 : 1.25 : 1.5, 1 : 1.25 : 3, 1 : 1.25 : 5, and 1 : 1.25 : 8 respectively.



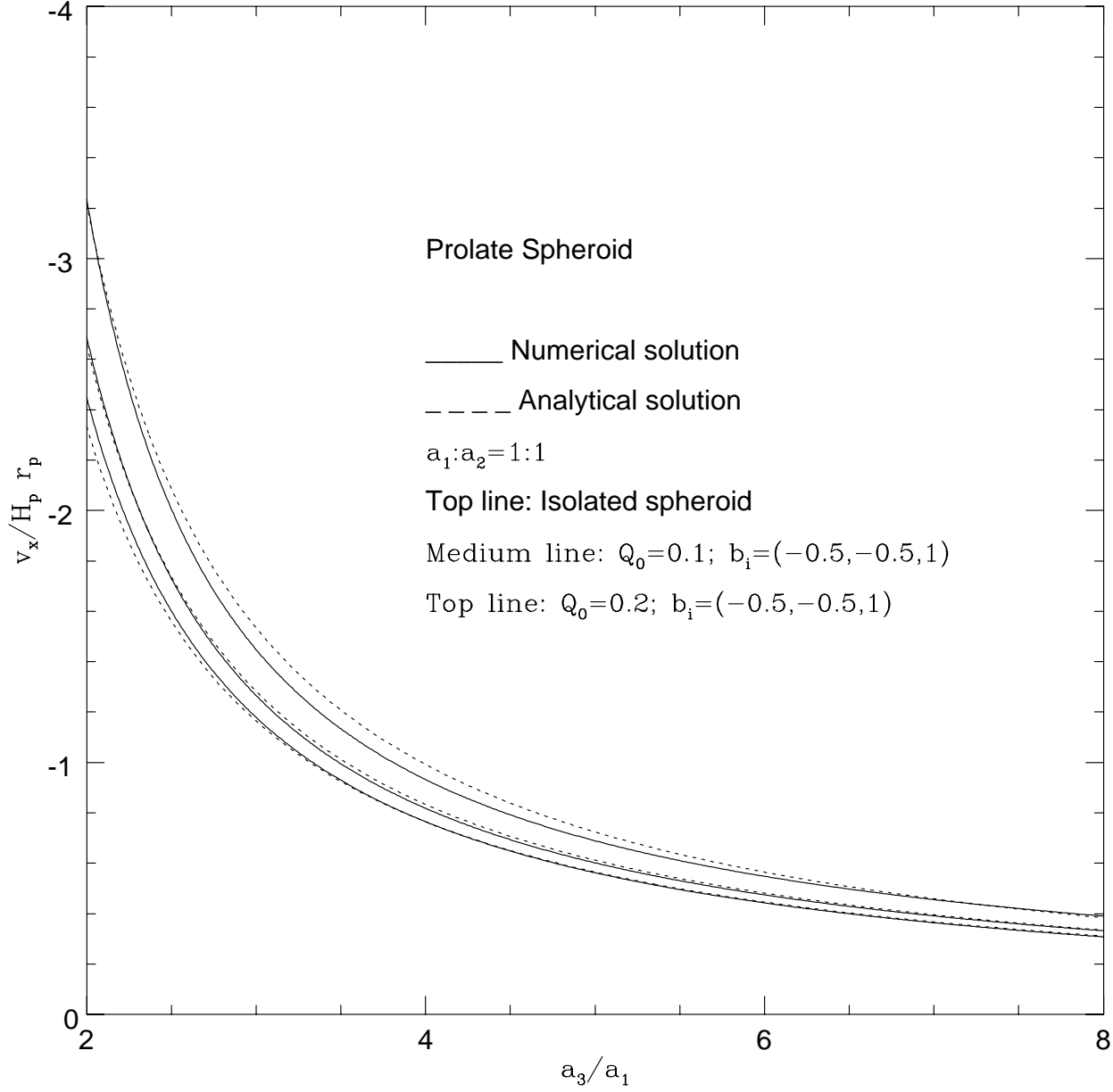
**Fig. 7** Comparison between density contrast predicted by spherical and oblate spheroidal models. The solid line represents the density contrast predicted by the spherical model, while the dotted, short-dashed, and long-dashed lines represents the prediction of the model with  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and initial axial ratio  $2 : 2 : 1$ ,  $4 : 4 : 1$ ,  $8 : 8 : 1$ , respectively.



**Fig. 8** Density contrast at virialization. The solid line refers to an *isolated* prolate spheroid.



**Fig. 9** Turnaround epoch for a prolate spheroid. The solid, short-dashed and long-dashed lines, represent respectively the time of turnaround for an *isolated* spheroid and for spheroids having  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$  and  $Q_0 = 0.2$ ,  $(-0.5, -0.5, 1)$ . The upper dotted line represents the value of the density contrast at turnaround for a spherical perturbation.



**Fig. 10** Axial velocity at collapse as function of the ratio of the initial value of the axes,  $a_3/a_1$ .

The solid lines represent the numerical results of the collapse velocity for a prolate spheroid, the dotted lines the result obtained from the approximate solution. The top curve represents the velocity for an *isolated* spheroid, the medium one the same quantity for a spheroid having  $Q_0 = 0.1$ ,  $b_i = (-0.5, -0.5, 1)$ , and the last bottom curve the velocity for a spheroid having  $Q_0 = 0.2$ , and  $b_i = (-0.5, -0.5, 1)$ .